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RESEARCH MEMORANDUM

EXPERIMENTAL PRESSURE DISTRIBUTION ON AN ASYMMETRICAL NONCONICAL BODY AT MACH NUMBER 1.90

By DeMarquis D. Wyatt

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Cleveland, Ohio

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NATIONAL ADVISORY COMMITTEE FOR AERONAUTICS
WASHINGTON
February 24, 1949

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EXPERIMENTAL PRESSURE DISTRIBUTION ON AN ASYMMETRICAL NONCONICAL BODY AT MACH NUMBER 1.90

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SUMMARY

An investigation of the pressure distribution on an asymmetrical nonconical body has been conducted at a Mach number of 1.90 over a wide range of angles of attack and yaw. The pressure distributions conformed to anticipated trends. Boundary-layer separation apparently occurred from the upper surface at angles of attack above 24° and from the lower surface at an angle of attack of -15°. No separation from the sides of the body was evident at angles of yaw up to 12°.

INTRODUCTION

Theoretical methods are available for the calculation of pressure distributions on conical bodies and axially symmetric nonconical bodies in a supersonic stream, but no satisfactory methods are available for the treatment of arbitrary nonconical bodies without axial symmetry. In order to determine the pressure distribution on a nonconical body without axial symmetry, a model was experimentally investigated. Data were obtained over a wide range of angles of attack and yaw at a Mach number of 1.90 in the NACA Lewis 18-by-18-inch supersonic wind tunnel.

APPARATUS AND PROCEDURE

The test-section Mach number in the 18-by-18-inch supersonic tunnel in the region in which the model was located was 1.90 ± 0.02, as determined by a calibration of the tunnel. Tunnel-inlet conditions were maintained at a stagnation temperature of 150° ± 10° F and a dew-point temperature of -10° ± 10° F. The Reynolds number of the model, based on the model length, was approximately 3.8×10^6.

Photographs of the brass model are presented in figure 1. A sketch of the model showing principal dimensions and typical cross sections is presented in figure 2. The length of the model over which pressures were measured was 13.50 inches. Static-pressure orifices of 0.013-inch diameter were located along several longitudinal body lines of the model. The orifice locations are given in table I in terms of the ratio x/L and the angle θ, where x is the distance from the tip of the model to the orifice, L is the length of the model over which pressures were measured (13.50 in.), and θ is the angle between the top of the model and the orifice measured in a clockwise direction looking forward. Pressures were recorded from a multiple-tube manometer board using tetrabromoethane as a fluid and were read to the nearest 0.05 inch of fluid.

The model was supported from the rear by a cylindrical body that was pinned to a strut passing through the bottom of the tunnel (fig. 1(a)). The strut was split and could be adjusted from outside the tunnel to vary the angle of attack of the model during operation of the tunnel. The angle of attack of the model was determined from cathetometer measurements taken during operation. For variations in angle of yaw, the model was rotated 90° relative to the position on the cylindrical body shown in figure 1(a).

The investigation was conducted at an angle of yaw of 0° over an angle-of-attack range from -15° to 30° and at 0°, 5°, and 10° angles of attack over an angle-of-yaw range from -15° to 15°. Adaptor mountings were inserted between the model and the support body to give the 5° and 10° angles of attack for the investigation of yaw effects at angles of attack. The model was centered in the tunnel at 0° deflection for all phases of the investigation in which the angle of yaw was varied and for runs at negative angles of attack and 0° angle of yaw. In order to avoid tunnel-wall interferences, the model was lowered about 3 inches in the tunnel for positive angle of attack at 0° angle of yaw.

RESULTS AND DISCUSSION

Data are presented in tables II to V in the form of pressure coefficient C_p at each orifice for each condition investigated. The pressure coefficient is defined by the equation

$$C_p = \frac{p-p_0}{q_0}$$

where p is the local surface pressure, p_0 is the free-stream static pressure, and q_0 is the free-stream dynamic pressure.

The data presented in table II were obtained with the model at two vertical positions in the tunnel. Pressure coefficients meas-
1025 ured at 0° angle of attack varied as much as 0.08 for corresponding orifices between the two runs. Check runs substantiated this discrepancy. The variable angle-of-yaw runs were made with the model centered in the tunnel in the same vertical position as for the negative angle-of-attack runs, but the data for 0° angle of yaw (tables III to V) show good agreement with the data obtained at positive angle of attack. Because of the agreement between the data for positive angles of attack and data for variable angles of yaw, the data in table II for negative angle of attack are believed to be incorrect.

Typical schlieren photographs of the model are presented in figure 3 for conditions of 0° angle of yaw and several angles of attack. An apparent pronounced boundary-layer separation from the top (expansion) surface of the model was observed at angles of attack of 30° and 24° (figs. 3(a) and 3(b), respectively). Inconsistent variations in the pressure coefficients measured on the upper surface that were observed for these conditions are attributed to the apparent separation.

The boundary layer did not appear to separate from the body at the lower angles of attack, although the layer was appreciably thickened about midway on the body at 18° angle of attack (fig. 3(c)). Below an angle of attack of 18°, no thickening of the boundary layer was evident (figs. 3(d) to 3(f)). The boundary-layer growth on the lower surface was moderate at -6° angle of attack (fig. 3(g)), but separation appeared to occur near the tip at -15° angle of attack (fig. 3(h)).

The apparent line of discontinuity in the separated region adjacent to the upper surface of the body at 24° angle of attack (fig. 3(b)) cannot be explained. This line was noticeable at 21° angle of attack and persisted up to 27° angle of attack. The line was not transient, being visible on the schlieren screen during steady observation of the flow.

The schlieren photographs in figure 4 are typical of those obtained for all runs at variable angles of yaw and 0° angle of attack. Operation up to angles of yaw of 12° caused no appreciable thickening or observable separation of the boundary layer.

Pressure distributions along longitudinal planes on the model are plotted in figure 5 from the data in table II for a representative range of angles of attack at 0° angle of yaw. Data for 0° angle of attack were taken from only the positive angle-of-attack run. The pressure-coefficient trends conformed to the anticipated trends. Because of flow expansion along the nonconical body, the pressures decreased in a rearward direction. Pressures were appreciably higher on the wedge-shaped surfaces at the rear of the body in comparison with pressures on the body nose because of the shock originating from the wedge. The wedge had no influence on the pressures on the lower part of the body.

Longitudinal pressure distributions are plotted in figures 6 to 8 for a range of angles of yaw at 0°, 5°, and 10° angles of attack, respectively. (See tables III to V.) Because of body symmetry about the vertical plane through the center line of the body, it was expected that the values of pressure coefficient measured at the intersection of this plane with the top and the bottom of the body would be the same for both positive and negative angles of yaw. The experimentally measured pressure coefficients were the same for positive and negative angles of yaw, which indicates uniform conditions in the tunnel air stream.

Radial pressure distributions at two locations on the body are presented in figures 9 to 12. Data for these figures were obtained from the faired curves of figures 5 to 8. The pressure distribution at $x/L = 0.148$ (section A-A, fig. 2) was qualitatively typical of the pressure distribution at any point on the body ahead of the wedge. The distribution at $x/L = 0.898$ (section E-E, fig. 2) was similarly typical of the flow over the body rearward of the wedge. Because of the body symmetry about the vertical center line, curves are presented for only the negative angles of yaw in figures 10 to 12; the curves of the data for positive angles of yaw are mirror images of the curves shown.

Pressure distributions on the flat wedge surface are indicated in figures 13 to 16 for representative experimental conditions. The rearward orifices were located on the right side of the wedge, but the appropriate data are transposed in these figures to indicate the pressures on the left wedge surface. A double set of values is given at one orifice location. The upper value was measured on the left and the lower value was measured on the right wedge surface.

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SUMMARY OF RESULTS

The following results were obtained from an investigation of the pressure distribution on an asymmetrical nonconical body at a Mach number of 1.90 and a Reynolds number of approximately 3.8×10^6:

1. Measured longitudinal pressure-distribution trends conformed to anticipated trends. Pressures decreased in a rearward direction on the body corresponding to a flow expansion about the nonconical body. The compression shock originating from the wedge increased pressures on the wedge surfaces in comparison with pressures on the body nose. The wedge had no influence on pressures on the lower surface of the body.

2. Apparent boundary-layer separation from the top surface of the body was observed at angles of attack above 24° and from the bottom surface at -15° angle of attack.

Lewis Flight Propulsion Laboratory,
National Advisory Committee for Aeronautics,
Cleveland, Ohio.

TABLE I - ORIFICE LOCATIONS ON MODEL

Radial location θ, (deg)	Longitudinal location, x/L								
0	0.074	0.185	0.296	0.408	0.518	0.630	[a]0.741	0.852	0.963
30	[a].889	[a].926	[a].963	-----	-----	-----	------	-----	-----
45	.111	.222	.333	.444	.556	.667	.778	[a].889	[a].926
60	[a].889	[a].926	[a].963	-----	-----	-----	------	-----	-----
180	.093	.204	.315	.426	.537	.648	.759	.870	.982
225	.130	.241	.352	.463	.574	.685	.796	.908	-----
270	.148	.259	.370	.481	.592	.704	.815	.926	-----
300	[a].852	-----	-----	-----	-----	-----	------	-----	-----
315	[a].852	-----	-----	-----	-----	-----	------	-----	-----
330	[a].852	-----	-----	-----	-----	-----	------	-----	-----
340	[a].815	[a].852	-----	-----	-----	-----	------	-----	-----
350	[a].778	[a].815	[a].852	-----	-----	-----	------	-----	-----
355	[a].778	[a].815	-----	-----	-----	-----	------	-----	-----

[a]Orifice on wedge surface.

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TABLE II - TABULATED PRESSURE COEFFICIENTS AT 0° YAW ANGLE FOR RANGE OF ANGLES OF ATTACK

Angle of attack, α deg		30	27	24	21	18	15	12	9	6	3	0	0	-3	-6	-9	-12	-15
φ (deg)	x/L	Pressure coefficient, C_p																
0	.074	-.114	-.126	-.099	-.048	-.033	-.011	-.008	-.005	.012	.009	-.028	.054	.082	.126	.144	.174	.226
	.184	-.196	-.113	-.077	-.053	-.014	-.012	-.008	-.008	.003	.015	.010	.026	.046	.071	.121	.170	.200
	.296	-.283	-.164	-.077	-.041	-.023	-.025	-.018	-.013	-.021	-.001	.016	.009	.024	.050	.080	.124	.189
	.408	-.282	-.177	-.086	-.067	-.028	-.025	-.017	-.015	-.012	-.010	.008	.006	.025	.044	.073	.116	.172
	.518	-.293	-.271	-.111	-.077	-.041	-.024	-.026	-.018	-.015	-.011	.004	.011	.018	.044	.078	.109	.162
	.630	-.302	-.304	-.144	-.087	-.049	-.034	-.033	-.031	-.015	-.021	-.014	.008	.015	.040	.070	.098	.156
	.741	-.288	-.345	-.125	-.009	.012	.014	.018	.017	.020	.025	.049	.064	.080	.107	.142	.181	.236
	.852	-.278	-.303	-.151	.013	.021	.009	.005	.007	.014	.018	.038	.078	.102	.134	.168	.213	.263
	.963	-.190	-.290	-.137	-.058	-.014	.008	.003	.014	.030	.026	.031	.052	.071	.099	.134	.173	.219
30	.889	-.227	-.293	-.229	-.191	-.199	-.029	.070	.073	.083	.087	.094	.138	.127	.125	.132	.148	.178
	.926	-.239	-.298	-.238	-.205	-.189	-.029	.050	.059	.073	.081	.091	.116	.127	.143	.150	.165	.191
	.963	-.237	-.283	-.243	-.213	-.177	-.050	.029	.037	.054	.066	.082	.109	.123	.133	.148	.164	.191
45	.111	-.241	-.236	-.208	-.176	-.142	-.093	-.045	-.021	.005	.003	.016	.040	.053	.077	.093	.090	.106
	.222	-.275	-.264	-.236	-.228	-.193	-.110	-.085	-.030	-.003	.012	.008	.021	.033	.042	.060	.088	.105
	.333	-.290	-.275	-.237	-.226	-.194	-.139	-.067	-.021	-.018	-.004	.016	.007	.014	.028	.041	.061	.097
	.444	-.297	-.280	-.237	-.231	-.178	-.116	-.049	-.040	-.023	-.014	.003	.006	.012	.022	.030	.048	.080
	.555	-.303	-.304	-.235	-.223	-.199	-.116	-.050	-.030	-.024	-.014	0	.010	.015	.031	.041	.057	.082
	.666	-.292	-.308	-.256	-.217	-.190	-.108	-.054	-.040	-.030	-.025	-.018	.006	.009	.019	.023	.040	.068
	.778	-.300	-.315	-.248	-.219	-.194	-.132	-.028	-.028	-.017	-.004	-.001	.015	.021	.028	.039	.054	.074
	.852	-.272	-.291	-.209	-.144	-.127	-.117	.099	.099	.105	.110	.128	.144	.137	.136	.138	.141	.159
	.889	-.274	-.298	-.213	-.123	-.095	-.086	.084	.086	.096	.101	.119	.147	.146	.148	.149	.157	.176
	.926	-.255	-.289	-.238	-.142	-.093	-.136	.060	.065	.080	.088	.098	.123	.124	.134	.144	.152	.174
	.963	-.246	-.289	-.230	-.139	-.114	-.116	.042	.050	.066	.078	.089	.116	.124	.133	.147	.162	.182
60	.889	-.246	-.289	-.227	-.099	-.064	-.070	.010	.089	.105	.108	.126	.147	.149	.148	.151	.151	.166
	.926	-.236	-.293	-.226	-.136	-.077	-.060	0	.065	.082	.089	.100	.123	.126	.124	.124	.127	.141
	.963	-.234	-.291	-.198	-.150	-.083	-.055	.002	.056	.070	.081	.088	.113	.118	.120	.127	.137	.153
180	.093	.677	.593	.518	.444	.399	.328	.261	.190	.133	.093	.054	.085	.055	.031	-.001	-.023	-.040
	.204	.595	.543	.486	.404	.319	.249	.194	.145	.094	.049	.021	.031	.011	-.004	-.012	-.039	-.056
	.315	.619	.526	.440	.359	.286	.224	.165	.110	.074	.041	.009	.019	.001	-.011	-.019	-.026	-.051
	.426	.561	.476	.399	.322	.251	.186	.134	.086	.049	.023	-.004	.004	-.013	-.023	-.026	-.040	-.055
	.537	.507	.454	.377	.302	.229	.168	.118	.075	.040	.015	-----	.004	-.012	-.018	-.025	-.040	-.059
	.648	.517	.436	.361	.289	.218	.160	.109	.068	.035	.013	-.003	.002	-.012	-.016	-.022	-.040	-.058
	.759	.496	.417	.340	.267	.200	.140	.094	.055	.022	.001	-.011	0	-.012	-.019	-.029	-.049	-.061
	.870	.503	.417	.342	.267	.204	.144	.097	.061	.032	.008	-.005	.015	.002	-.009	-.017	-.036	-.052
	.982	.490	.417	.348	.277	.202	.139	.092	.052	.026	.009	-.003	.010	.005	.004	-.003	-.017	-.040
225	.130	.282	.241	.201	.184	.151	.117	.093	.082	.072	.051	.035	.051	.026	.007	-.032	-.070	-.108
	.241	.246	.207	.171	.130	.088	.059	.045	.042	.039	.026	.015	.025	.009	-.015	-.045	-.082	-.110
	.352	.229	.177	.138	.101	.072	.043	.025	.016	.019	.021	.007	.017	.001	-.021	-.064	-.077	-.115
	.463	.186	.144	.105	.067	.036	.012	-.008	-.002	.002	.006	0	.005	-.009	-.032	-.052	-.072	-.107
	.574	.179	.136	.095	.055	.024	.002	-.012	-.012	-.004	.003	.002	.007	-.010	-.029	-.047	-.061	-.094
	.685	.146	.103	.067	.030	0	-.024	-.024	-.024	-.014	-.008	-.002	.005	-.008	-.025	-.046	-.068	-.093
	.796	.125	.084	.048	.015	-.015	-.038	-.045	-.043	-.021	-.014	-.008	.010	-.007	-.030	-.048	-.068	-.098
	.908	.162	.129	.099	.071	.021	-.011	-.014	-.013	.010	.019	.024	.022	.002	-.021	-.039	-.053	-.087
270	.148	-.219	-.215	-.193	-.171	-.153	-.115	-.080	-.045	-.003	.001	.027	.029	.030	.035	.032	.006	-.012
	.259	-.194	-.198	-.191	-.187	-.177	-.156	-.106	-.064	-.035	-.004	-.005	.005	.012	.008	-.006	-.013	-.021
	.370	-.179	-.179	-.173	-.168	-.174	-.153	-.117	-.068	-.028	-.005	.013	.019	.016	.010	-.002	-.018	-.023
	.481	-.174	-.167	-.167	-.154	-.165	-.146	-.113	-.075	-.038	-.016	-.002	.004	.002	.001	-.016	-.027	-.031
	.592	-.177	-.145	-.160	-.157	-.157	-.150	-.120	-.081	-.045	-.021	-.008	.004	.003	-.008	-.029	-.035	-.050
	.704	-.202	-.155	-.163	-.173	-.161	-.159	-.123	-.093	-.041	-.025	-.016	.004	.002	-.004	-.019	-.042	-.062
	.815	-.202	-.147	-.175	-.179	-.155	-.136	-.132	-.075	-.046	-.037	-.017	-.005	-.007	-.010	-.022	-.039	-.052
	.926	-.132	-.043	-.042	-.052	-.032	-.001	.027	.067	.091	.101	.103	.117	.104	.089	.056	.020	-.008
300	.852	-.125	-.025	-.041	-.052	-.087	-.099	.017	.102	.126	.133	.128	.154	.153	.150	.148	.149	.157
315	.852	-.135	-.042	-.075	-.068	-.102	-.108	.003	.102	.118	.122	.118	.154	.141	.147	.157	.161	.175
330	.852	-.176	-.066	-.121	-.094	-.193	-.063	.088	.085	.093	.096	.092	.126	.127	.141	.155	.161	.183
340	.815	-.141	-.100	-.155	-.140	-.176	.021	.073	.061	.064	.069	.067	.137	.146	.151	.154	.171	.204
	.852	-.164	-.098	-.161	-.150	-.168	.042	.075	.067	.072	.070	.072	.106	.115	.137	.154	.168	.195
350	.778	-.097	-.151	-.128	-.146	-.060	.047	.046	.041	.042	.042	.060	.085	.086	.101	.118	.143	.180
	.815	-.056	-.197	-.129	-.143	-.034	.063	.057	.052	.050	.054	.051	.131	.121	.131	.145	.174	.226
	.852	-.082	-.192	-.141	-.148	-.021	.056	.045	.043	.046	.045	.057	.094	.114	.139	.163	.187	.222
355	.778	-.063	-.225	-.102	-.091	.006	.047	.043	.038	.036	.036	.054	.077	.089	.109	.131	.163	.206
	.815	-.014	-.241	-.108	-.070	.032	.050	.047	.041	.039	.045	.048	.118	.112	.130	.153	.189	.245

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TABLE III - TABULATED PRESSURE COEFFICIENTS AT 0° ANGLE OF ATTACK FOR RANGE OF YAW ANGLES

Angle of yaw, Ψ deg		12	9	6	3	0	-3	-6	-9	-12
θ (deg)	x/L	Pressure coefficient, C_p								
0	.074	-.134	-.072	-.007	.044	.051	.030	-.018	-.080	-.134
	.185	-.152	-.101	-.036	.015	.025	.003	-.043	-.101	-.152
	.296	-.150	-.119	-.059	-.009	.004	-.018	-.062	-.106	-.147
	.408	-----	-----	-.061	-.015	0	-.020	-.063	-.102	-.139
	.518	-.133	-.100	-.062	-.019	.004	-.017	-.052	-.088	-.128
	.630	-.121	-.099	-.071	-.022	-.011	-.040	-.092	-.120	-.143
	.741	-.186	-.180	-.152	-----	.041	-.077	-.162	-.180	-.194
	.852	-.167	-.144	-.093	-.013	.034	-.025	-.102	-.140	-.161
	.963	-.142	-.086	-.025	.016	.034	.011	-.040	-.094	-.137
30	.889	-.063	-.017	.032	.070	.101	.136	.172	.213	.259
	.926	-.048	.015	.044	.076	.096	.118	.149	.187	.234
	.963	-.025	.016	.044	.068	.085	.109	.140	.179	.224
45	.111	-.096	-.028	-.003	.024	.036	.054	.076	.099	.126
	.222	-.110	-.054	-.020	.004	.018	.036	.055	.075	.109
	.333	-.143	-.025	-.016	-.006	.001	.017	.035	.057	.083
	.444	-.170	-.038	-.020	-.011	-.003	.006	.022	.038	.061
	.555	-.185	-.052	-.023	-.009	-.002	.008	.020	.034	.062
	.666	-.190	-.074	-.030	-.019	-.015	-.002	.015	.029	.052
	.778	-.164	-.086	-.034	-.012	-.006	0	.006	.019	.039
	.852	-.048	.017	.057	.088	.122	.159	.201	.251	.303
	.889	-.132	-.048	.055	.093	.127	.155	.191	.234	.285
	.926	-.141	-.044	.043	.074	.104	.132	.169	.214	.262
	.963	-.057	-.024	.047	.074	.100	.128	.163	.203	.249
60	.889	-.040	.078	.081	.107	.134	.161	.199	.250	.302
	.926	-.085	.033	.055	.083	.114	.146	.185	.233	.280
	.963	-.096	.043	.053	.073	.095	.123	.161	.204	.246
180	.093	.001	.028	.054	.072	.066	.063	.055	.036	.010
	.204	-----	-.005	.011	.019	.026	.022	.014	-.008	-.027
	.315	-.034	-.016	.004	.013	.014	.017	-.005	-.018	-.041
	.426	-.053	-.033	-.018	-.001	-.002	-.009	-.014	-.032	-.054
	.537	-.061	-.039	-.021	-.015	-.008	-.010	-.017	-.040	-.065
	.648	-.069	-.045	-.023	-.006	-.008	-.010	-.020	-.044	-.071
	.759	-----	-----	-----	-----	-----	-----	-----	-----	-----
	.870	-.065	-.039	-.019	-.007	-.008	-.016	-.028	-.049	-.073
	.982	-.058	-.037	-.019	-.004	.001	-.004	-.019	-.043	-.072
225	.130	.084	.087	.080	.062	.042	.018	-.005	-.027	-.065
	.241	.060	.052	.040	.036	.020	.004	-.023	-.053	-.068
	.352	.041	.038	.034	.025	.020	-.011	-.033	-.054	-.067
	.463	-----	-----	-----	-----	-----	-----	-----	-----	-----
	.574	.016	.006	.006	.005	-.002	-.013	-.031	-.050	-.061
	.685	.001	.001	.005	.002	-.010	-.023	-.043	-.056	-.063
	.796	.017	.024	.028	.028	.011	-.008	-.030	-.048	-.059
	.908	-.023	-.014	-.004	.006	.008	.005	-.005	-.024	-.039
270	.148	.145	.124	.086	.048	.025	.009	-.006	-.010	-.033
	.259	.137	.083	.047	.025	.003	-.009	-.017	-.026	-.041
	.370	.125	.086	.049	.024	.010	-.007	-.009	-.022	-.034
	.481	.103	.061	.036	.013	-.007	-.014	-.020	-.030	-.046
	.592	.095	.057	.024	.003	-.013	-.016	-.023	-.032	-.050
	.704	.078	.041	.018	0	-.014	-.018	-.024	-.039	-.052
	.815	.072	.039	.014	-.002	-.018	-.021	-.025	-.031	-.042
	.926	.263	.216	.170	.134	.096	.072	.055	.052	.068
300	.852	.255	.251	.209	.175	.130	.112	.098	.097	-.072
315	.852	.313	.258	.203	.169	.132	.093	.070	.012	-.035
330	.852	.273	.224	.175	.137	.099	.066	.019	-.046	-.076
340	.815	.245	.200	.156	.121	.072	.033	-.017	-.055	-.087
	.852	.237	.194	.152	.117	.080	.048	.008	-.048	-.091
350	.778	.209	.178	.142	.113	.054	.011	-.034	-.091	-.142
	.815	.213	.174	.136	.097	.058	.019	-.015	-.125	-.221
	.852	.196	.160	.122	.090	.058	.028	0	-.188	-.229
355	.778	.183	.160	.128	.093	.048	.001	-.135	-.224	-.237
	.815	-----	.146	.119	.091	.058	.017	-.158	-.190	-.218

TABLE IV - TABULATED PRESSURE COEFFICIENTS AT 5° ANGLE OF ATTACK FOR RANGE OF YAW ANGLES

Angle of yaw, Ψ deg		12	9	6	3	0	-3	-6	-9	-12
θ (deg)	x/L	Pressure coefficient, C_p								
0	.074	-.115	-.066	-.017	.027	.033	.014	-.014	-.057	-.102
	.185	-.111	-.070	-.028	.006	.016	.001	-.028	-.061	-.095
	.296	-.102	-.071	-.038	-.004	.012	-.002	-.024	-.052	-.079
	.408	-.106	-.066	-.036	-.004	.009	.001	-.017	-.045	-.082
	.518	-.096	-.062	-.033	-.009	.008	-.001	-.020	-.052	-.082
	.630	-.086	-.054	-.027	-.008	.004	-.014	-.030	-.054	-.088
	.741	-.133	-.103	-.075	-.019	.056	-.027	-.051	-.079	-.111
	.852	-.111	-.082	-.042	.008	.051	.010	-.019	-.053	-.086
	.963	-.108	-.052	-.003	.030	.052	.037	.009	-.041	-.096
30	.889	-.050	-.017	.070	.103	.128	.148	.183	.213	.249
	.926	-.084	-.021	.058	.088	.110	.131	.167	.197	.232
	.963	-.089	-.013	.058	.078	.096	.107	.137	.164	.197
45	.111	-.047	-.020	.006	.020	.026	.028	.044	.065	.077
	.222	-.063	-.018	.001	.012	.020	.028	.039	.058	.086
	.333	-.073	-.011	-.002	.003	.010	.015	.022	.035	.056
	.444	-.093	-.029	-.007	0	.004	.002	.010	.021	.032
	.555	-.100	-.036	-.008	.005	.004	.006	.012	.020	.033
	.666	-.094	-.042	-.014	-.005	.002	.006	.011	.017	.032
	.778	-.082	-.039	-.005	.007	.010	.003	.003	.007	.018
	.852	.034	.106	.119	.121	.151	.177	.211	.242	.287
	.889	.044	.087	.112	.117	.138	.160	.197	.228	.273
	.926	-.012	.044	.083	.097	.121	.145	.181	.213	.250
	.963	-.039	.043	.068	.079	.102	.123	.159	.194	.231
60	.889	.102	.128	.118	.117	.147	.169	.202	.230	.274
	.926	.085	.088	.086	.096	.122	.145	.180	.210	.248
	.963	.051	.049	.067	.081	.109	.134	.173	.211	.251
180	.093	.083	.103	.124	.136	.126	.115	.112	.093	.069
	.204	.036	.062	.084	.093	.102	.102	.097	.087	.077
	.315	.046	.056	.063	.072	.080	.077	.076	.071	.051
	.426	.021	.032	.048	.055	.056	.059	.067	.070	.027
	.537	.008	.021	.037	.052	.065	.059	.057	.042	.026
	.648	.008	.027	.044	.048	.059	.058	.055	.042	.025
	.759	-.012	.012	.027	.038	.046	.047	.049	.036	.019
	.870	-----	-----	-----	-----	-----	-----	-----	-----	-----
	.982	.024	.039	.051	.051	.058	.060	.060	.040	.003
225	.130	.178	.167	.149	.113	.073	.037	-.001	-.041	-.085
	.241	-----	-----	-----	-----	-----	-----	-----	-----	-----
	.352	.153	.122	.096	.092	.037	.002	-.030	-.080	-.089
	.463	.127	.105	.083	.056	.026	-.009	-.047	-.084	-.093
	.574	.122	.101	.083	.061	.031	-.004	-.042	-.091	-.119
	.685	.123	.093	.077	.051	.020	-.016	-.057	-.109	-.137
	.796	.070	.069	.067	.043	.015	-.022	-.065	-.113	-.124
	.908	.149	.141	.124	.103	.072	.029	-.009	-.049	-.067
270	.148	.118	.090	.067	.031	.011	.002	-.017	-.048	-.063
	.259	.102	.064	.025	.007	0	-.008	-.033	-.042	-.068
	.370	.111	.065	.030	.017	.006	-.013	-.012	-.029	-.053
	.481	.083	.046	.025	.005	-.002	-.003	-.018	-.042	-.053
	.592	.076	.039	.018	.004	-.008	-.004	-.016	-.028	-.053
	.704	.067	.032	.006	-.007	-.010	-.005	-.011	-.026	-.058
	.815	.057	.026	.007	-.005	-.010	-.007	-.014	-.027	-.069
	.926	.218	.184	.163	.138	.118	.102	.088	.048	-.041
300	.852	.194	.194	.203	.189	.165	.152	.161	.132	.072
315	.852	.306	.262	.223	.186	.154	.148	.157	.153	.063
330	.852	.269	.225	.187	.153	.124	.116	.093	.045	.004
340	.815	.235	.199	.159	.128	.098	.079	.054	.023	-.024
	.852	.227	.185	.151	.122	.099	.082	.042	-.005	-.053
350	.778	.201	.169	.135	.107	.076	.042	.025	-.011	-.046
	.815	.195	.161	.130	.104	.080	.048	.019	-.028	-.083
	.852	.170	.135	.108	.087	.076	.063	.026	-.054	-.118
355	.778	.166	.141	.114	.093	.066	.031	-.020	-.101	-.148
	.815	.149	.124	.104	.086	.067	.038	-.055	-.102	-.143

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TABLE V - TABULATED PRESSURE COEFFICIENTS AT 10° ANGLE OF ATTACK FOR RANGE OF YAW ANGLES

Angle of yaw, ψ deg		12	9	6	3	0	-3	-6	-9	-12
φ (deg)	x/L	Pressure coefficient, C_p								
0	.074	-.123	-.088	-.051	-.012	0	-.015	-.036	-.073	-.112
	.185	-.110	-.080	-.044	-.026	-.012	-.035	-.046	-.072	-.101
	.296	-----	-.046	-.046	-.030	-.018	-.032	-.053	-.077	-.104
	.408	-.102	-.077	-.048	-.025	-.015	-.032	-.043	-.065	-.097
	.518	-.100	-.072	-.045	-.018	-.012	-.021	-.030	-.050	-.086
	.630	-.100	-.068	-.038	-.029	-.024	-.027	-.043	-.070	-.104
	.741	-.114	-.084	-.032	.011	.026	.007	-.038	-.081	-.114
	.852	-.111	-.090	-.047	0	-.014	0.	-.049	-.082	-.112
	.963	-.140	-.097	-.042	0	.006	-.006	-.053	-.108	-.139
30	.889	-.012	.025	.042	.077	.076	.090	.121	.147	.175
	.926	-.036	.022	.069	.070	.064	.072	.097	.127	.156
	.963	-.053	.024	.038	.050	.042	.057	.080	.103	.134
45	.111	-.072	-.055	-.038	-.021	-.022	-.028	-.021	-.017	-.016
	.222	-----	-----	-----	-----	-----	-----	-----	-----	-----
	.333	-.087	-.054	-.030	-.029	-.046	-.045	-.045	-.045	-.014
	.444	-.087	-.061	-.043	-.031	-.038	-.051	-.053	-.053	-.045
	.555	-.081	-.062	-.041	-.040	-.032	-.038	-.047	-.049	-.039
	.666	-.082	-.067	-.049	-.059	-.044	-.044	-.053	-.060	-.048
	.778	-.068	-.056	-.041	-.052	-.022	-.039	-.065	-.070	-.057
	.852	.067	.066	.073	.059	.100	.120	.141	.151	.150
	.889	.068	.059	.056	.063	.080	.099	.124	.142	.163
	.926	.057	.068	.059	.040	.066	.083	.113	.143	.171
	.963	.051	.038	.034	.028	.052	.069	.094	.126	.157
60	.889	.050	.022	.029	.022	.090	.104	.123	.127	.128
	.926	.048	-.010	-.037	-.002	.067	.086	.109	.130	.147
	.963	.026	-.039	-.037	-.011	.054	.076	.104	.137	.167
180	.093	.165	.169	.181	.206	.204	.188	.187	.167	.155
	.204	.106	.116	.143	.148	.148	.141	.143	.141	.127
	.315	.101	.113	.118	.120	.126	.124	.129	.134	.127
	.426	.090	.089	.091	.097	.105	.105	.097	.095	.089
	.537	.061	.066	.077	.088	.098	.109	.116	.096	.093
	.648	.056	.062	.074	.081	.089	.080	.072	.063	.061
	.759	.039	.053	.056	.058	.068	.067	.067	.062	.057
	.870	.044	.052	.061	.072	.077	.075	.065	.059	.054
	.982	.083	.090	.102	.112	.116	.116	.108	.102	.088
225	.130	.257	.211	.175	.139	.078	.017	-.035	-.083	-.136
	.241	.208	.195	.148	.094	.034	-.024	-.082	-.135	-.175
	.352	.220	.175	.122	.071	.024	-.031	-.094	-.152	-.191
	.463	.187	.141	.091	.046	-.004	-.057	-.107	-.162	-.183
	.574	.172	.133	.088	.040	-.007	-.063	-.114	-.173	-.206
	.685	.157	.119	.085	.024	-.026	-.081	-.133	-.197	-.221
	.796	.143	.096	.060	.013	-.034	-.089	-.148	-.207	-.202
	.908	.161	.129	.091	.049	-.006	-.061	-.133	-.161	-.138
270	.148	.063	.014	-.001	-.036	-.056	-.067	-.102	-.145	-.167
	.259	.005	-.015	-.054	-.076	-.074	-.097	-.125	-.167	-.190
	.370	.036	-.012	-.051	-.062	-.073	-.103	-.124	-.151	-.170
	.481	.013	-.031	-.061	-.075	-.083	-.104	-.137	-.140	-.179
	.592	-.003	-.042	-.067	-.084	-.088	-.093	-.122	-.140	-.162
	.704	-.023	-.057	-.076	-.089	-.097	-.102	-.104	-.125	-.146
	.815	-.031	-.066	-.084	-.088	-.082	-.091	-.099	-.119	-.174
	.926	.103	.061	.039	.051	.052	.013	-.014	-.065	-.202
300	.852	.074	.075	.118	.125	.090	.026	.031	.039	.017
315	.852	.200	.189	.166	.135	.100	.109	.089	.087	.095
330	.852	.200	.170	.142	.110	.092	.092	.063	.047	.021
340	.815	.159	.144	.114	.081	.064	.068	-.040	-----	-.022
	.852	.168	.139	.114	.083	.067	.055	-.025	-.013	-.052
350	.778	.124	.109	.086	.050	.041	.036	.004	-.028	-.061
	.815	.134	.116	.088	.063	.054	.042	-.005	-.038	-.087
	.852	.118	.089	.061	.042	.040	.017	-.022	-.082	-.125
355	.778	.105	.087	.068	.039	.042	.024	-.022	-.072	-.102
	.815	.087	.078	.063	.044	.044	.020	-.039	-.095	-.130

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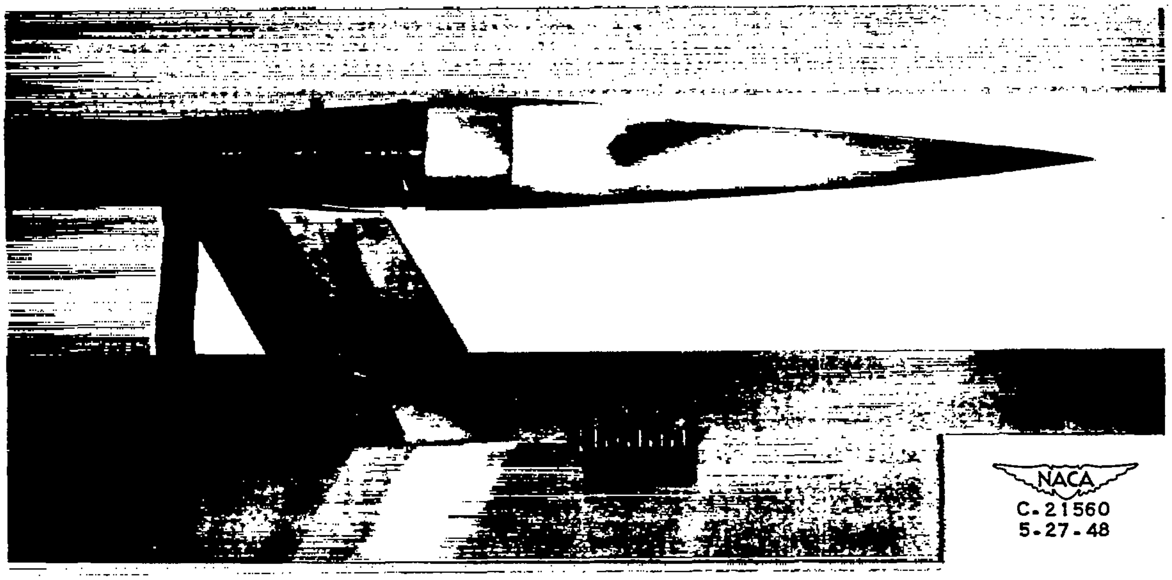
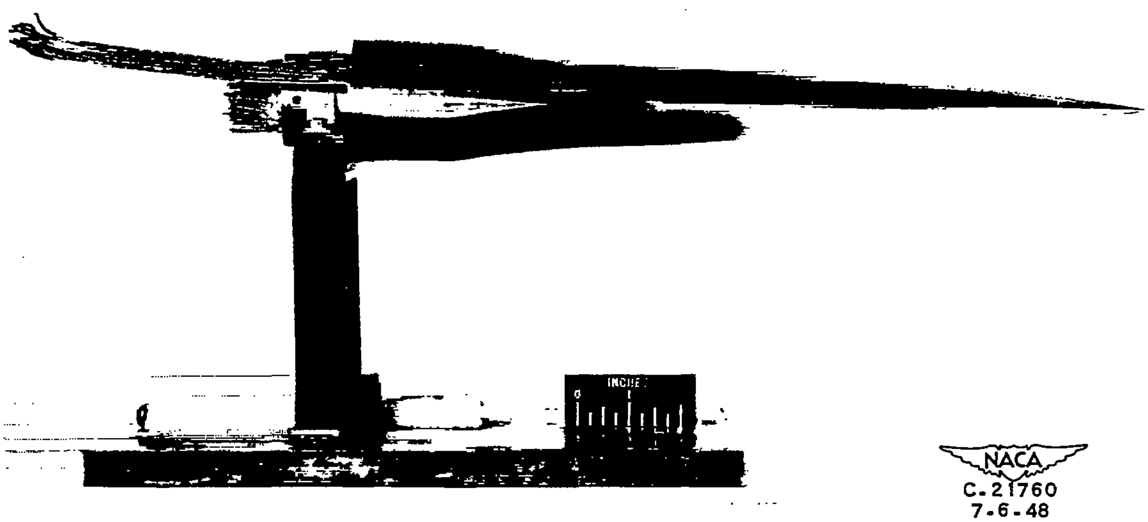


(a) Side view showing method of support.



(b) Top view.

Figure 1. - Photographs of model used in investigation.

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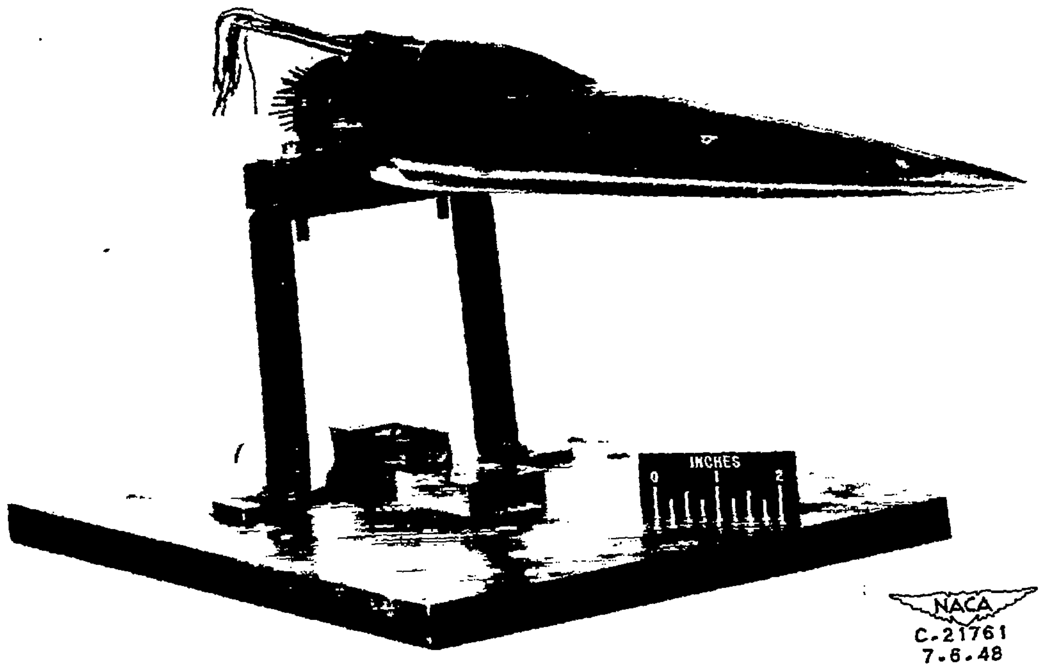
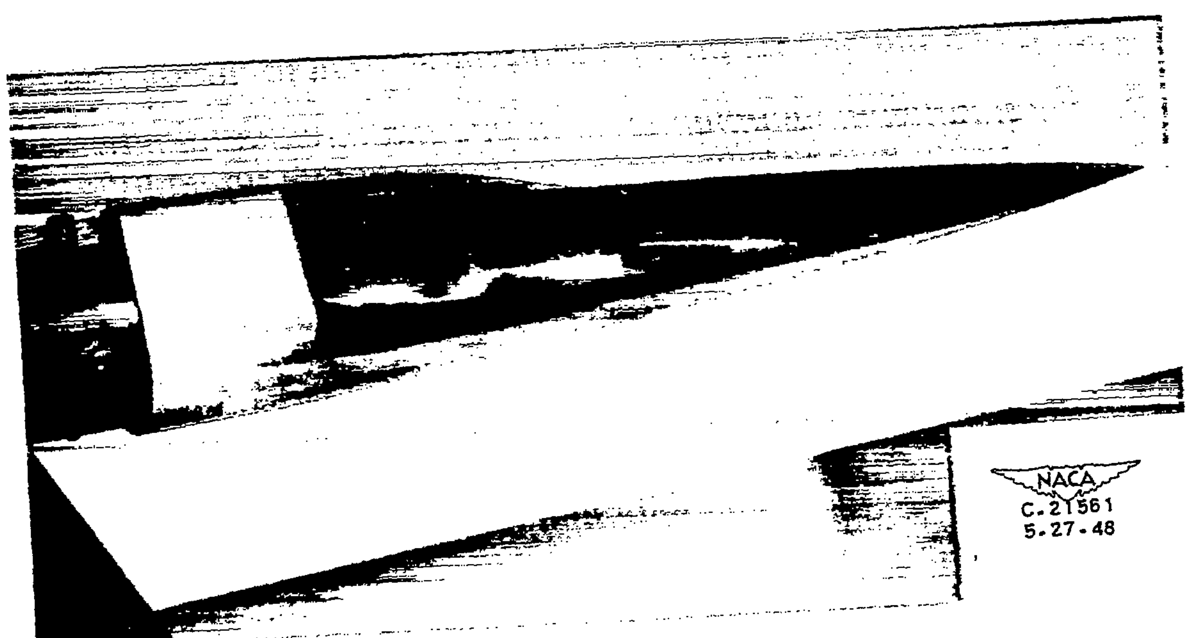
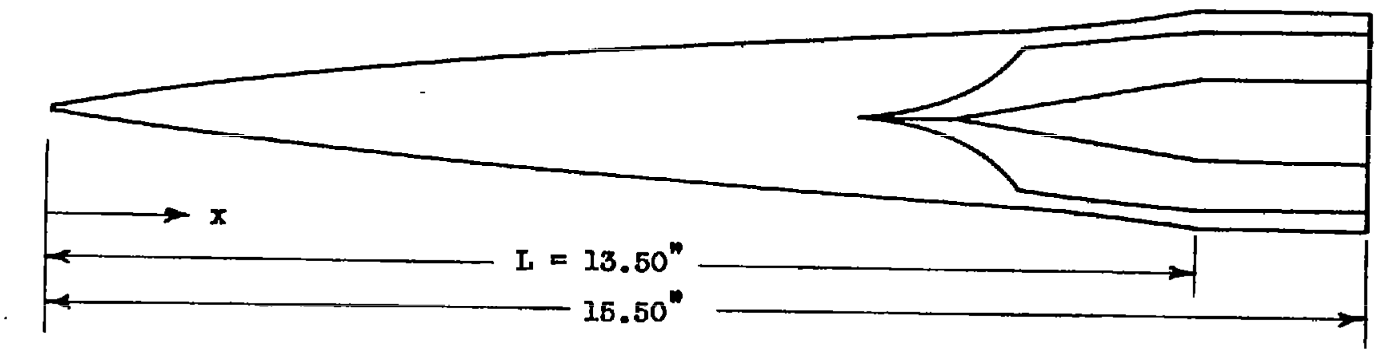


(c) Three-quarter front view.

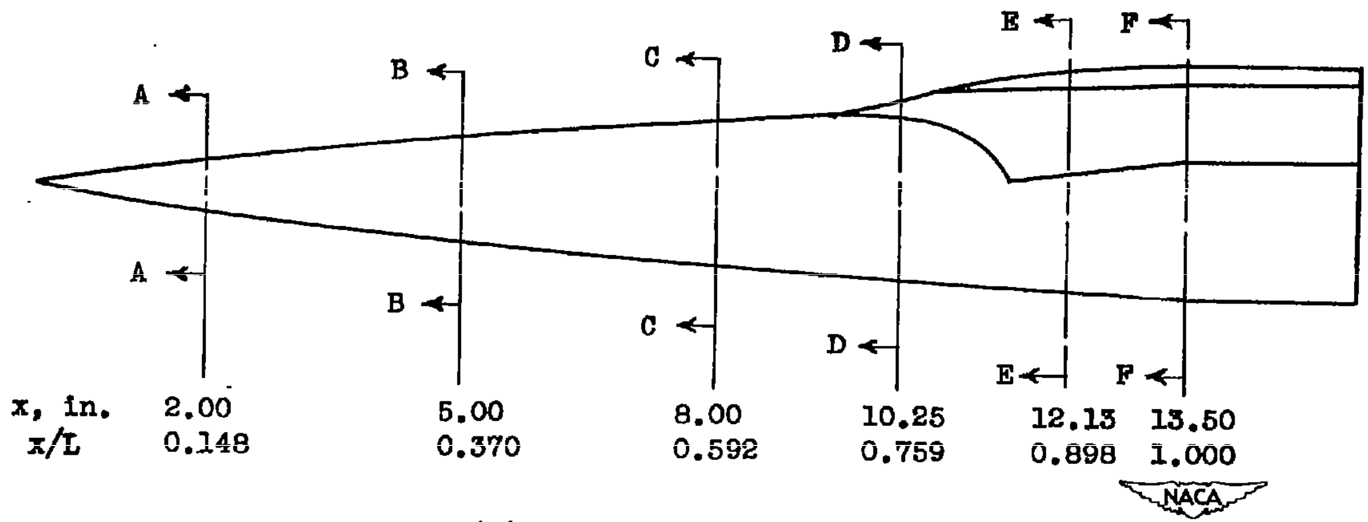


(d) Three-quarter close-up rear view.

Figure 1. - Concluded. Photographs of model used in investigation.



(a) Top view, half size.



(b) Side view, half size.

Figure 2. - Sketch of model showing principal dimensions and typical cross sections.

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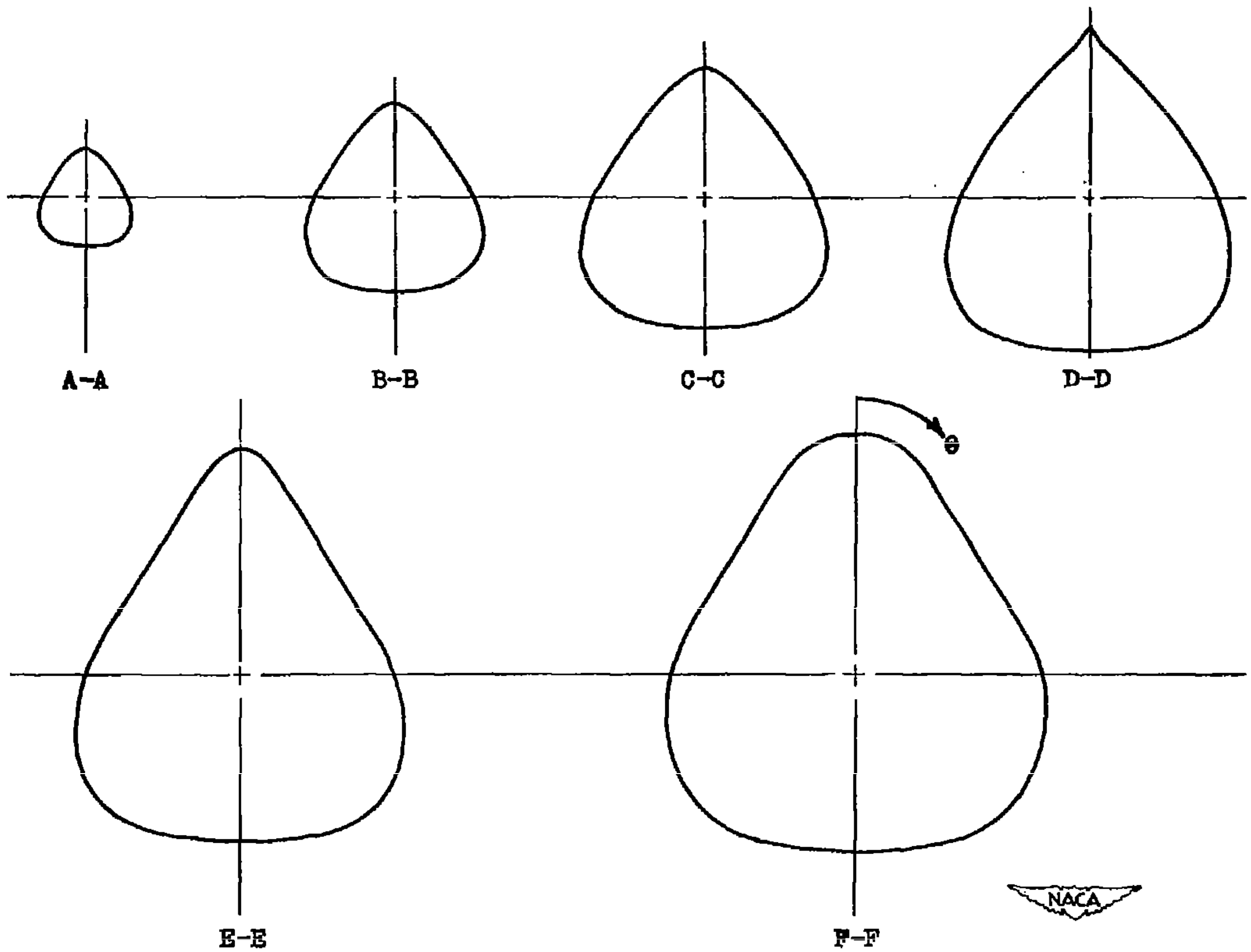
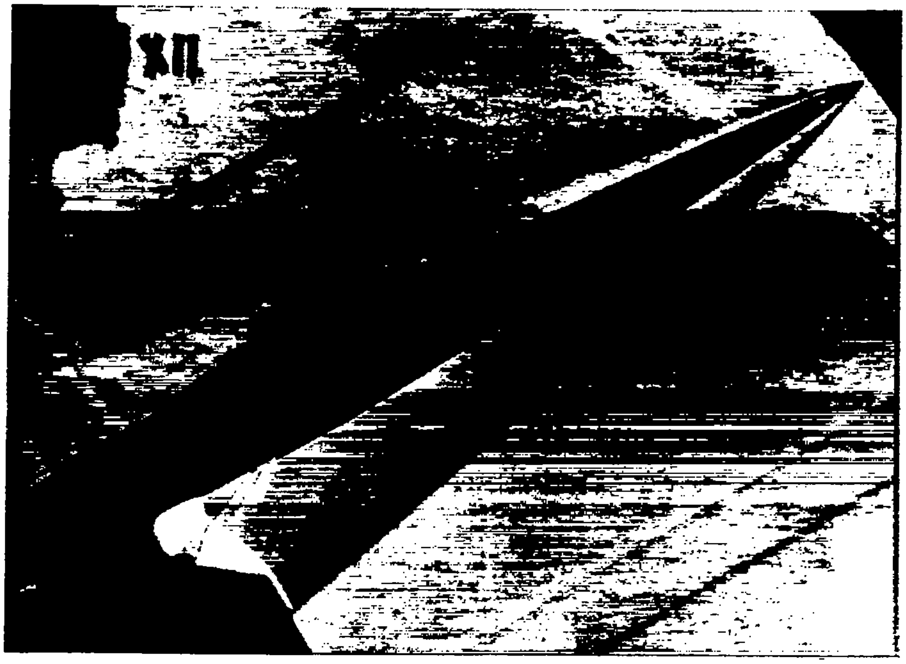
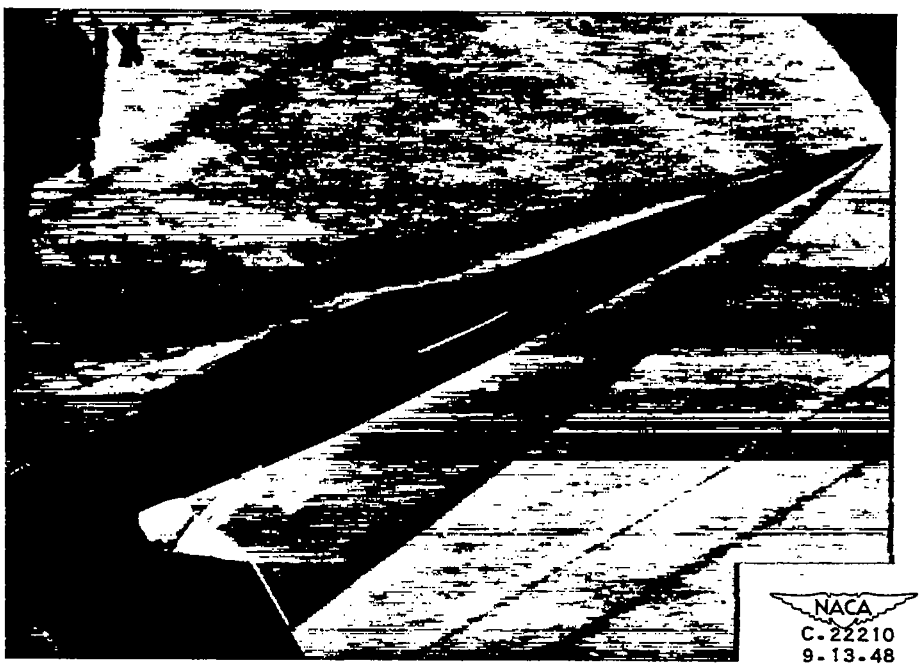


(c) Typical cross sections, full size (fig. 2(b)).

Figure 2. - Concluded. Sketch of model showing principal dimensions and typical cross sections.



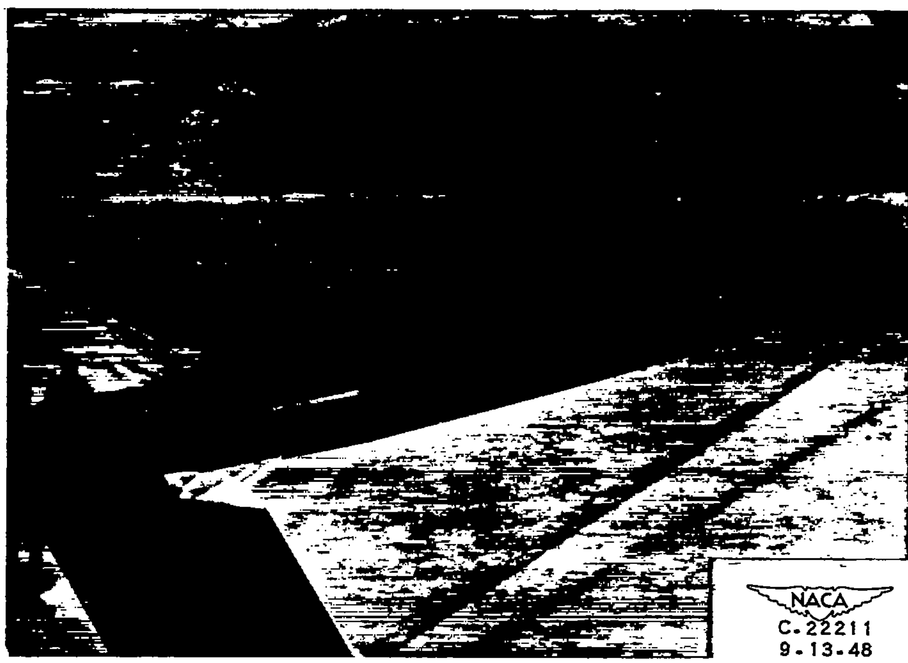
(a) Angle of attack, 30°.



(b) Angle of attack, 24°.

Figure 3. - Schlieren photographs of model at 0° angle of yaw.

(c) Angle of attack, 18°.



(d) Angle of attack, 12°.

Figure 3. - Continued. Schlieren photographs of model at 0° angle of yaw.

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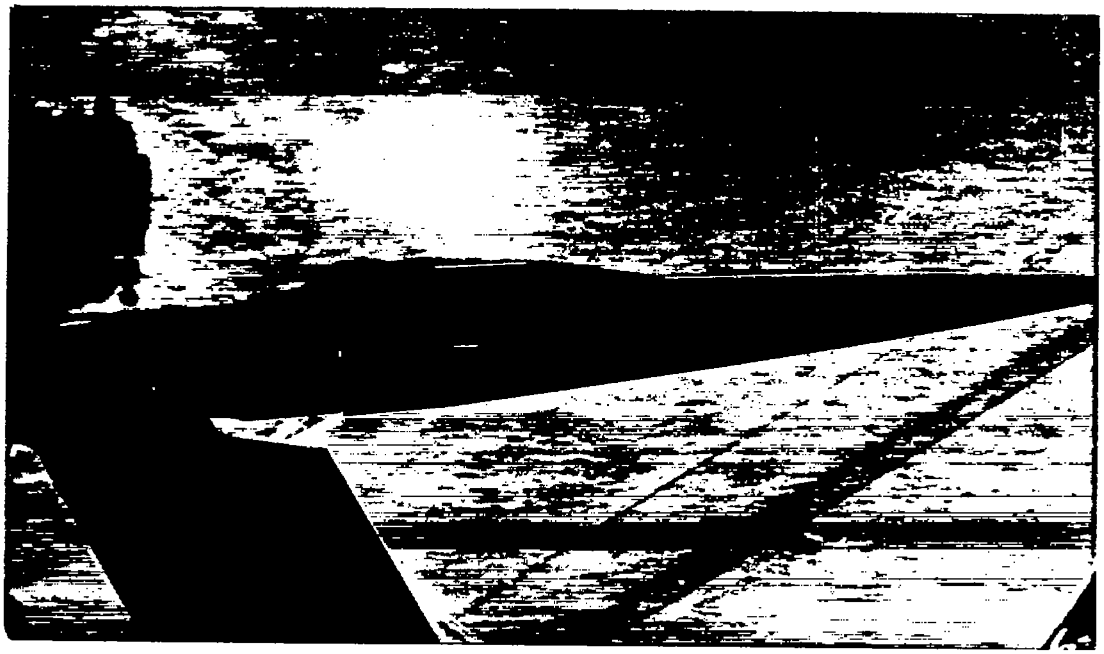
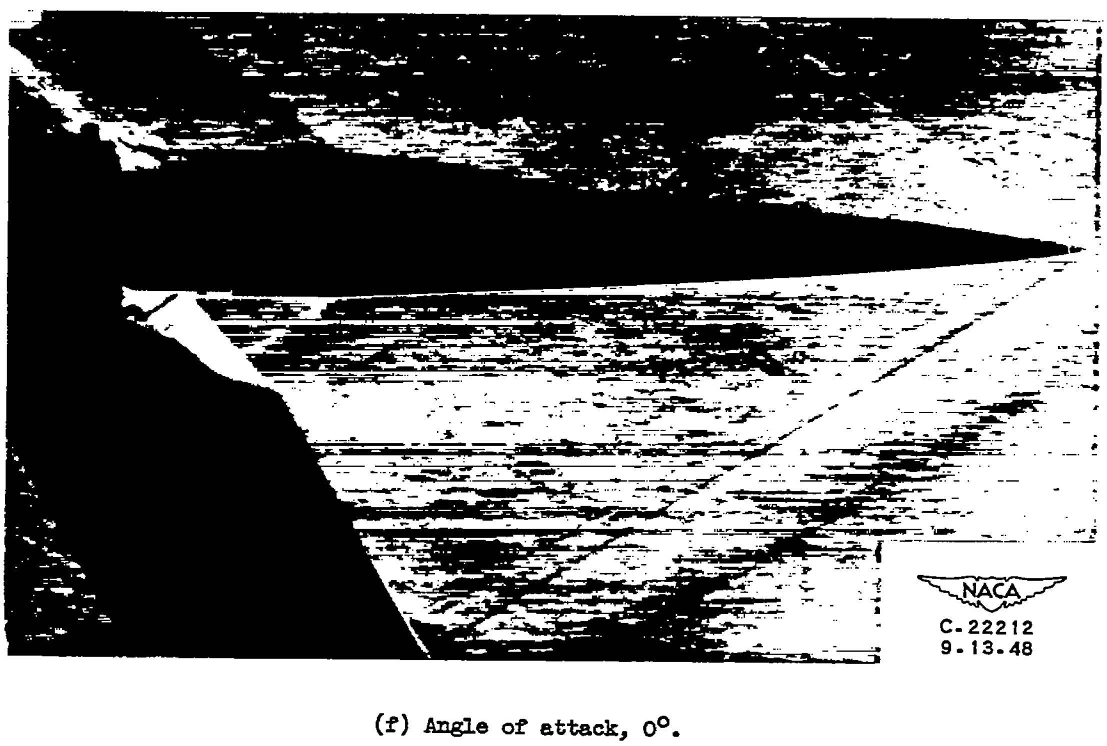


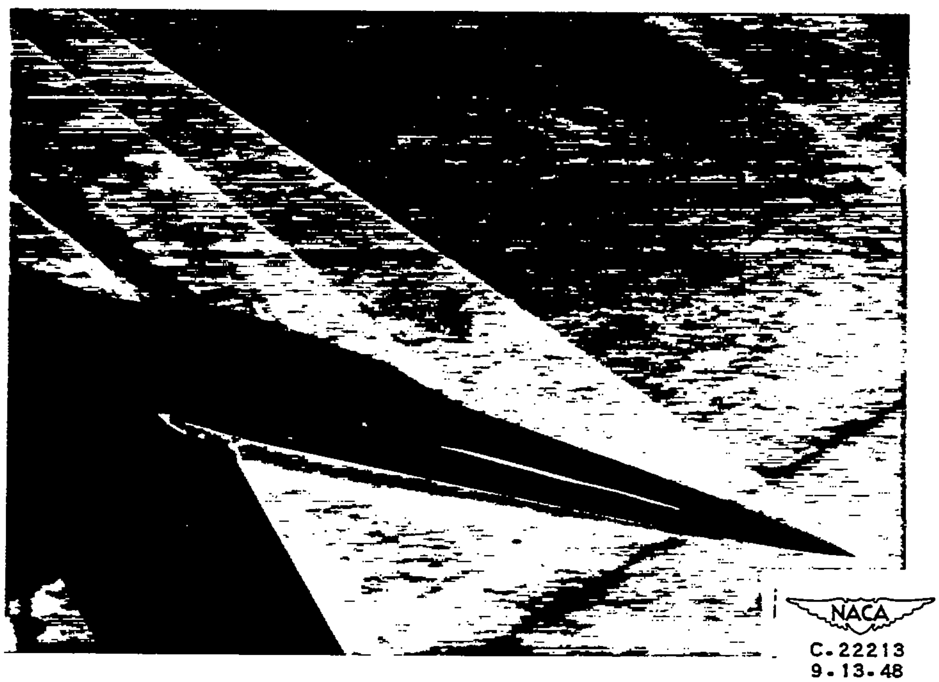
(e) Angle of attack, 6°.



(f) Angle of attack, 0°.

Figure 3. - Continued. Schlieren photographs of model at 0° angle of yaw.

(g) Angle of attack, -6°.



(h) Angle of attack, -15°.

Figure 3. - Concluded. Schlieren photographs of model at 0° angle of yaw.

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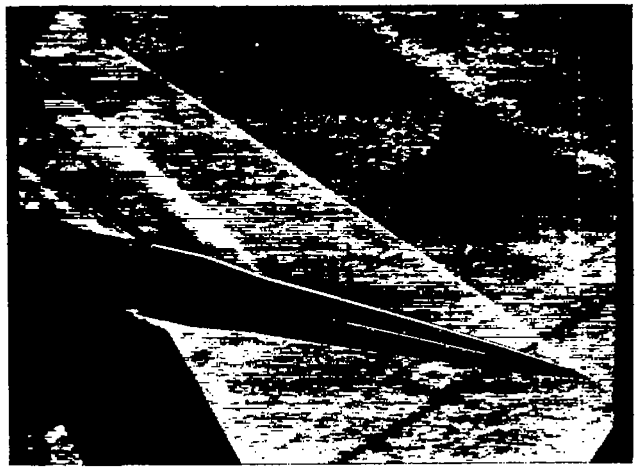
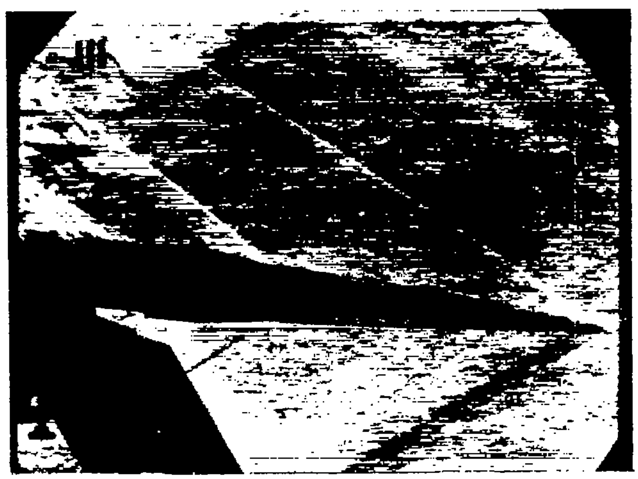
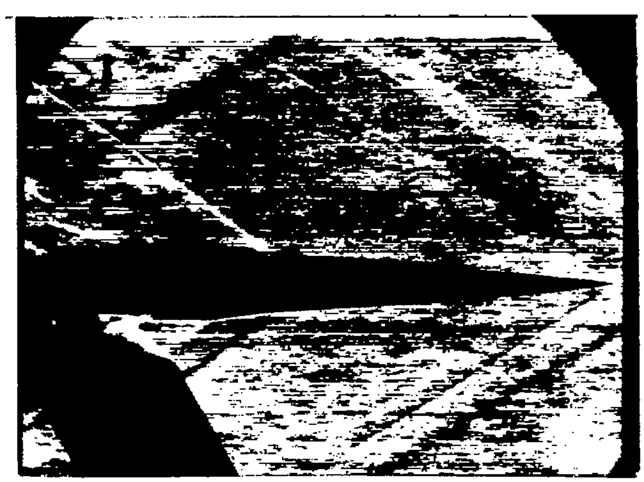


(a) Angle of yaw, 12°.



(b) Angle of yaw, 6°.



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(c) Angle of yaw, 0°.

Figure 4. - Schlieren photographs of model at 0° angle of attack.

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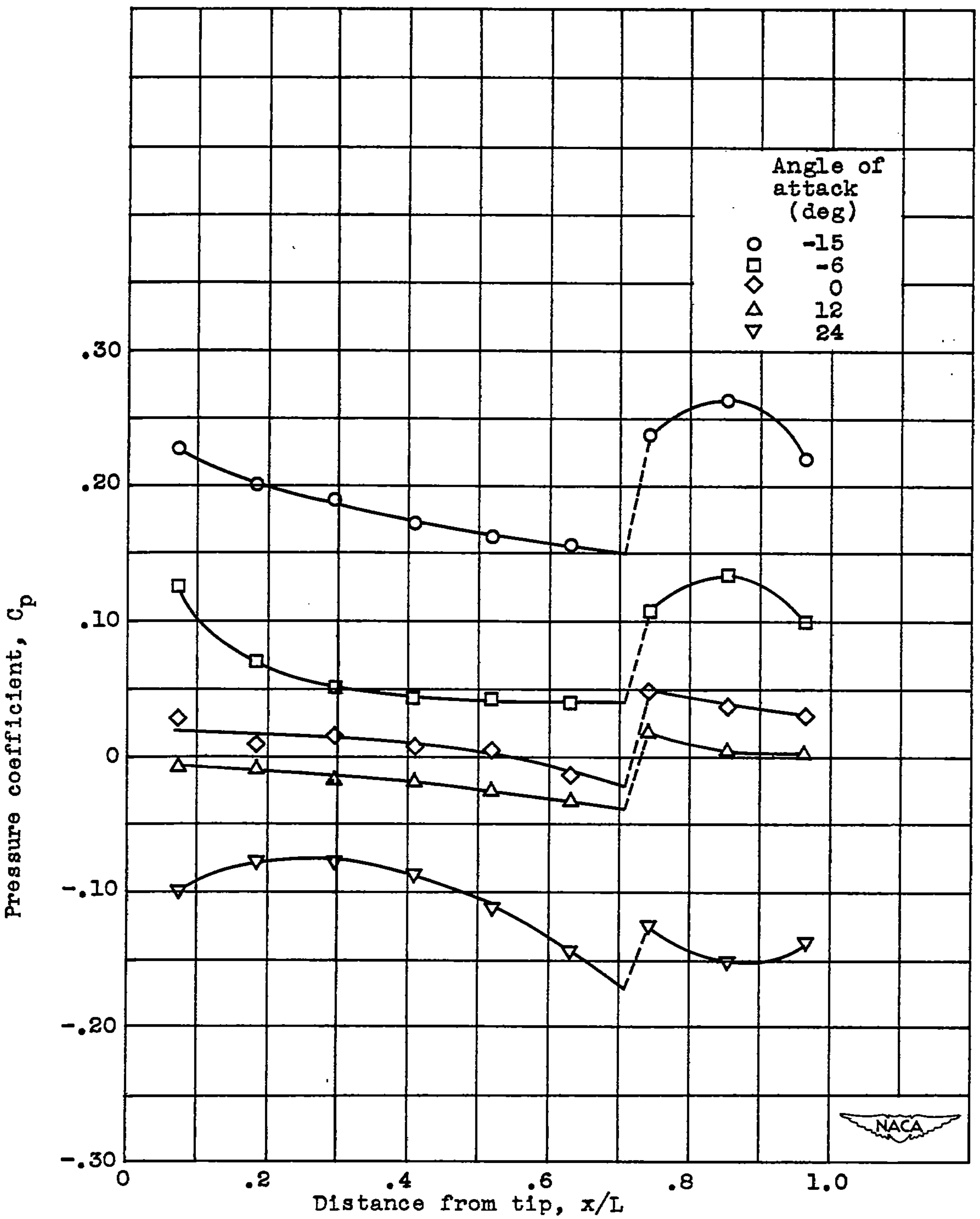

(a) $\theta = 0^{\circ}$ longitudinal plane.

Figure 5. - Pressure distributions along longitudinal planes at 0° yaw angle for range of angles of attack.

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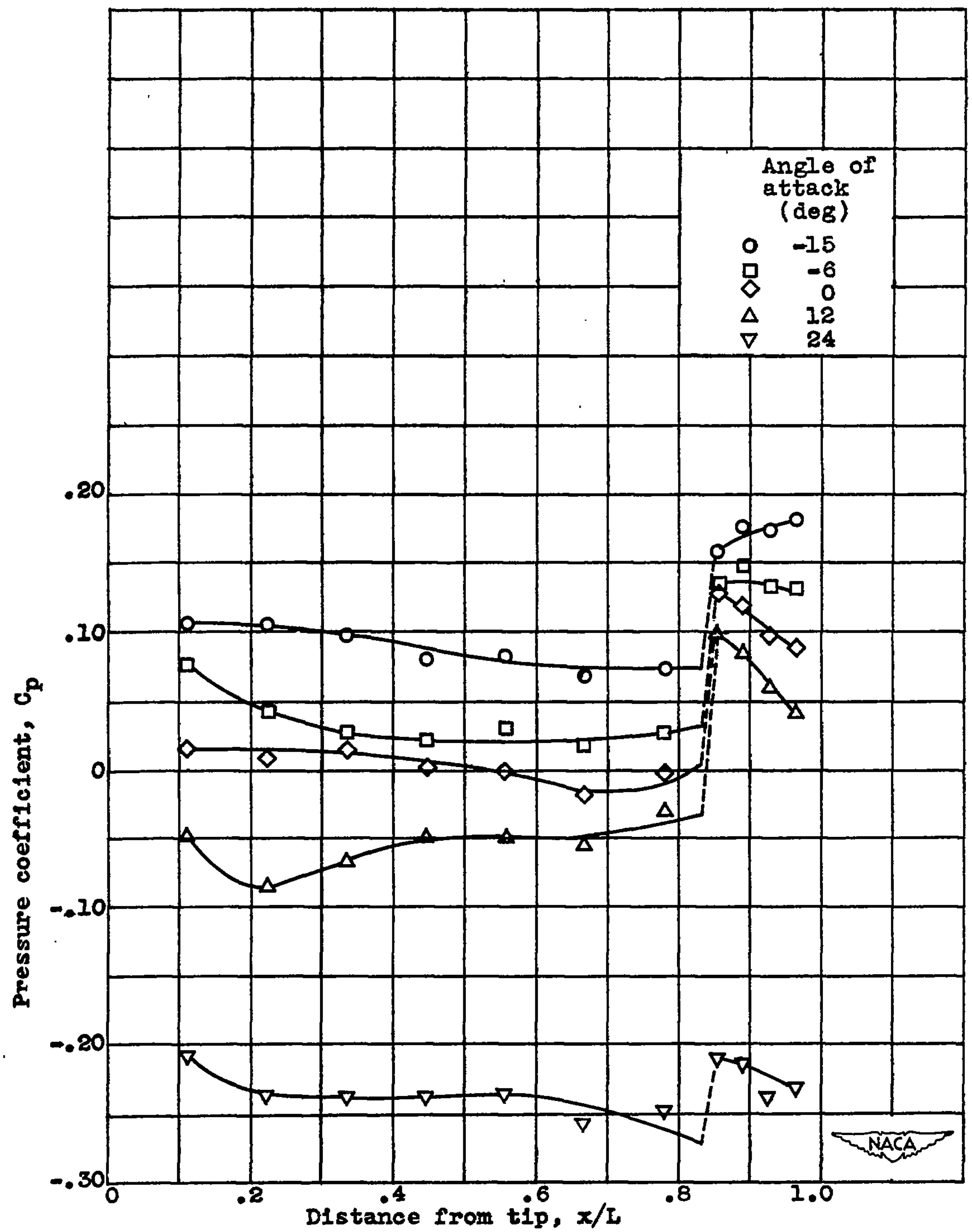
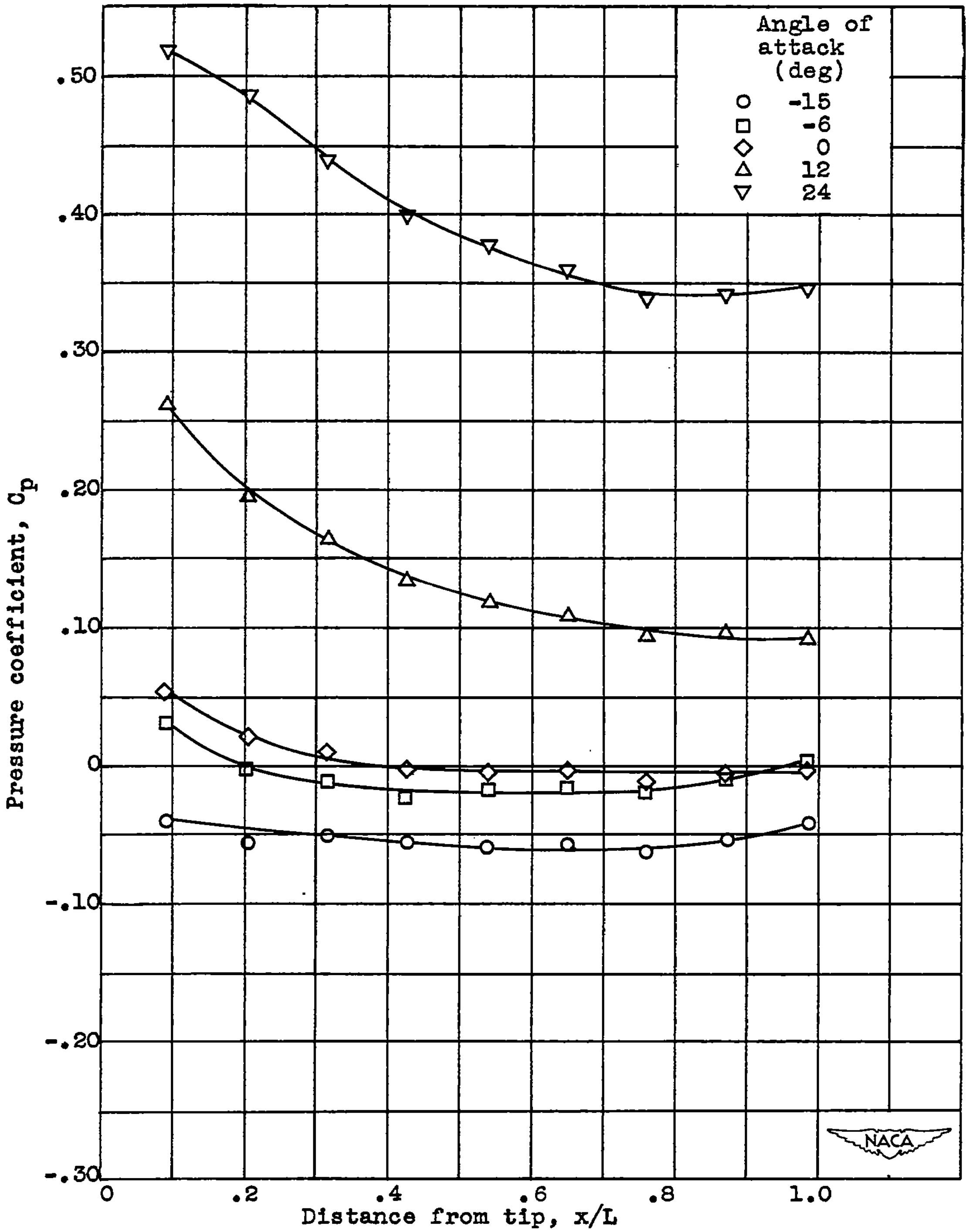


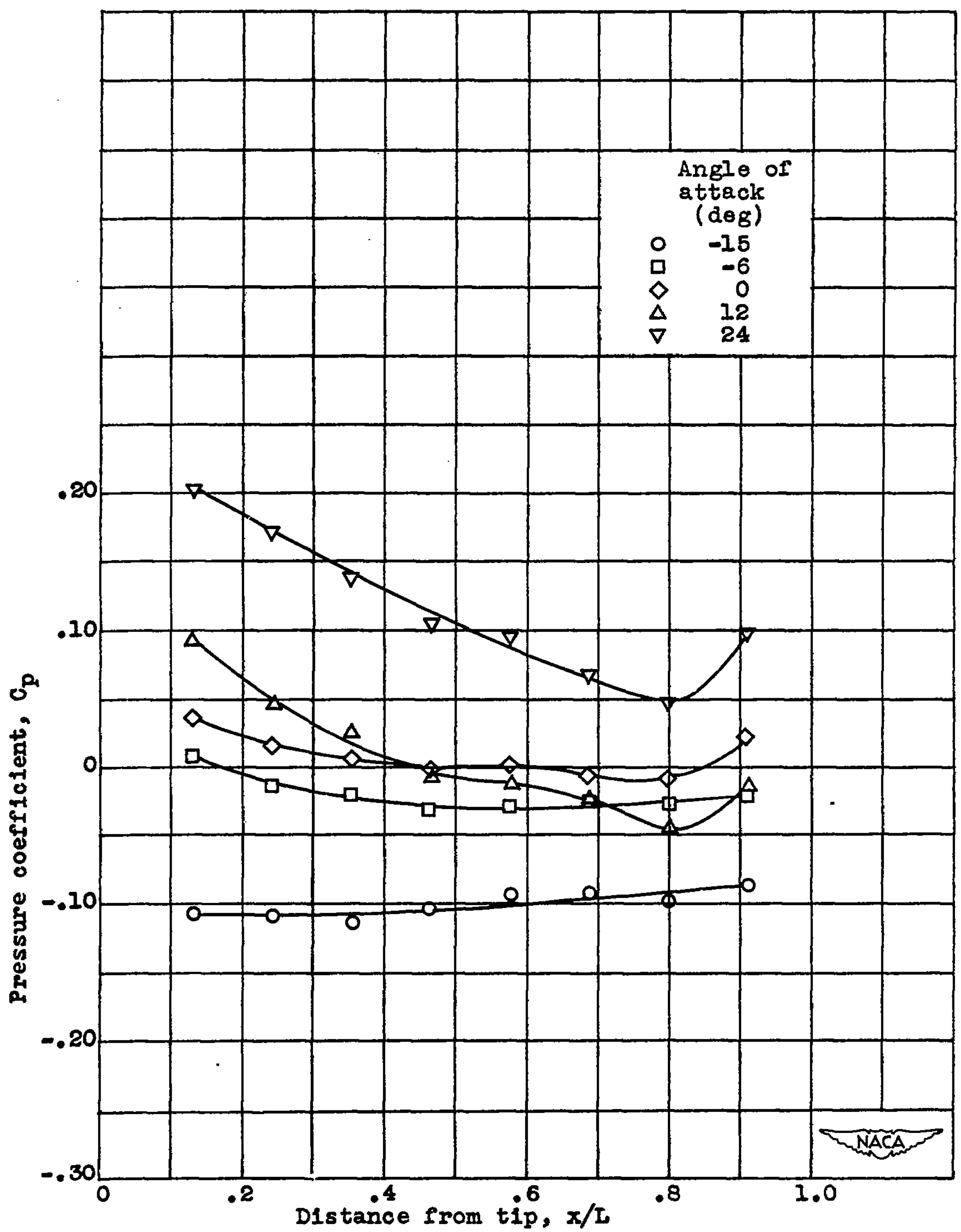
(b) $\theta = 45^{\circ}$ longitudinal plane.

Figure 5. - Continued. Pressure distributions along longitudinal planes at 0° yaw angle for range of angles of attack.



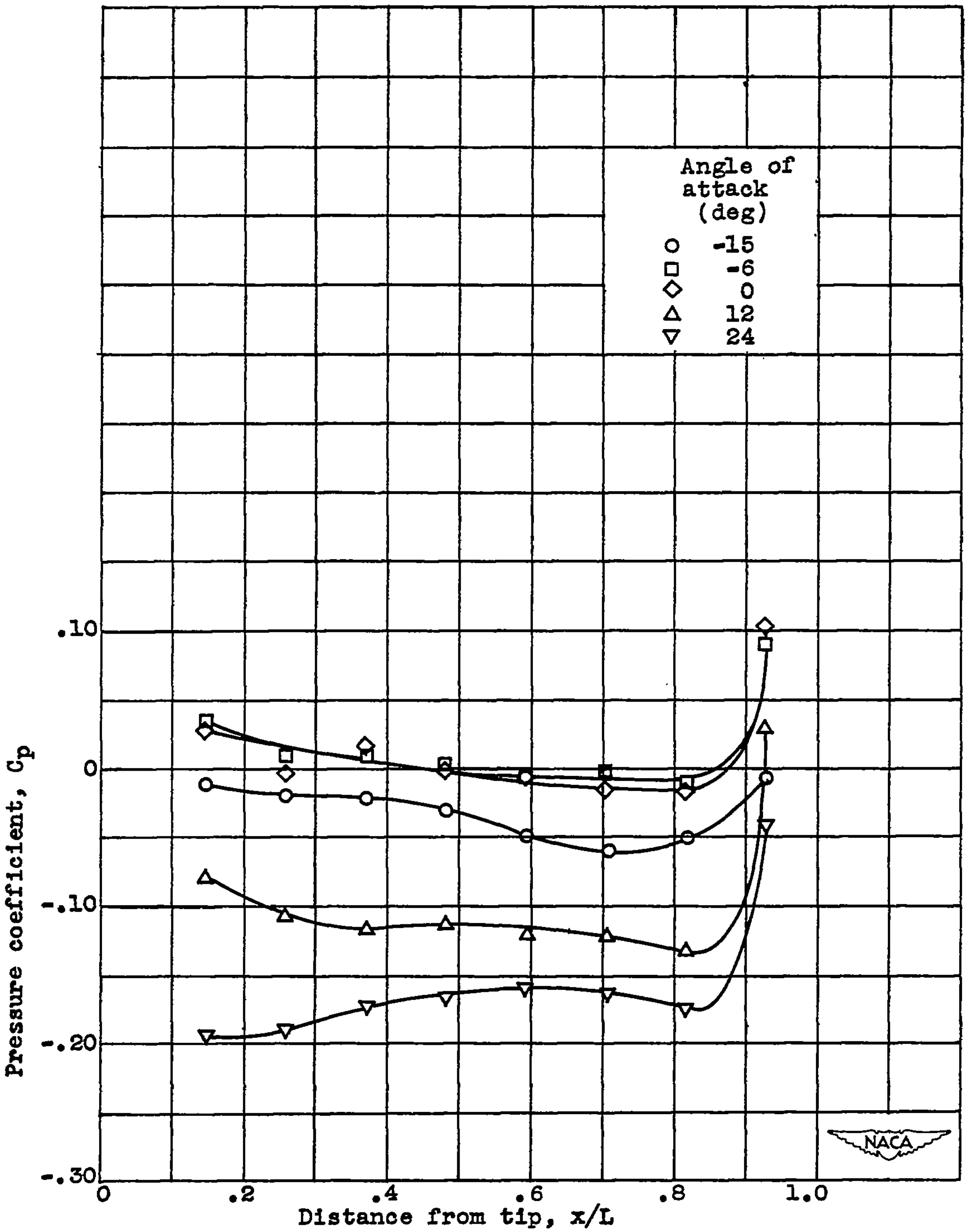
(c) $\theta = 180^\circ$ longitudinal plane.

Figure 5. - Continued. Pressure distributions along longitudinal planes at 0° yaw angle for range of angles of attack.



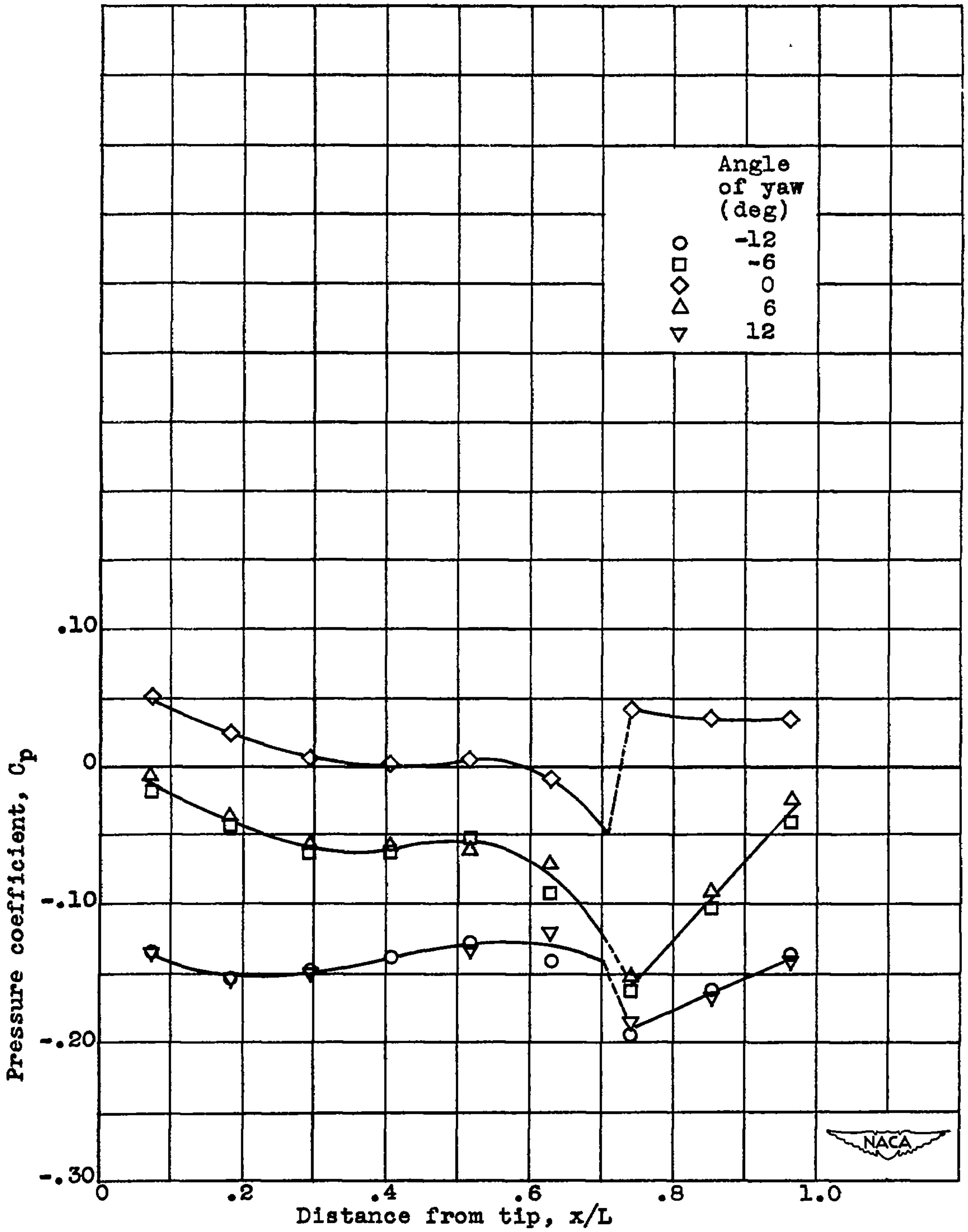
(d) θ = 225° longitudinal plane.

Figure 5. - Continued. Pressure distributions along longitudinal planes at 0° yaw angle for range of angles of attack.



(e) θ = 270° longitudinal plane.

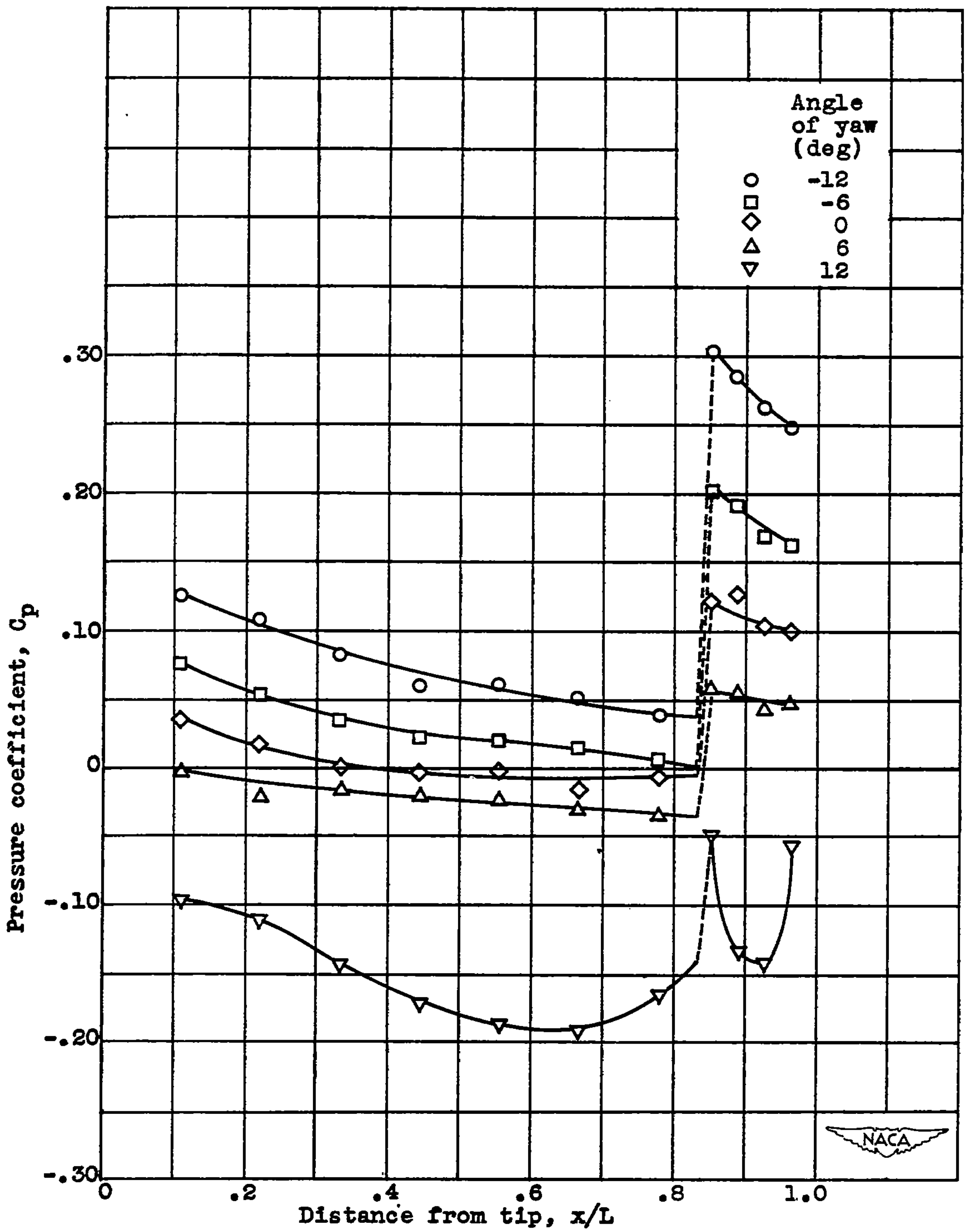
Figure 5. - Concluded. Pressure distributions along longitudinal planes at 0° yaw angle for range of angles of attack.



(a) $\theta = 0^\circ$ longitudinal plane.

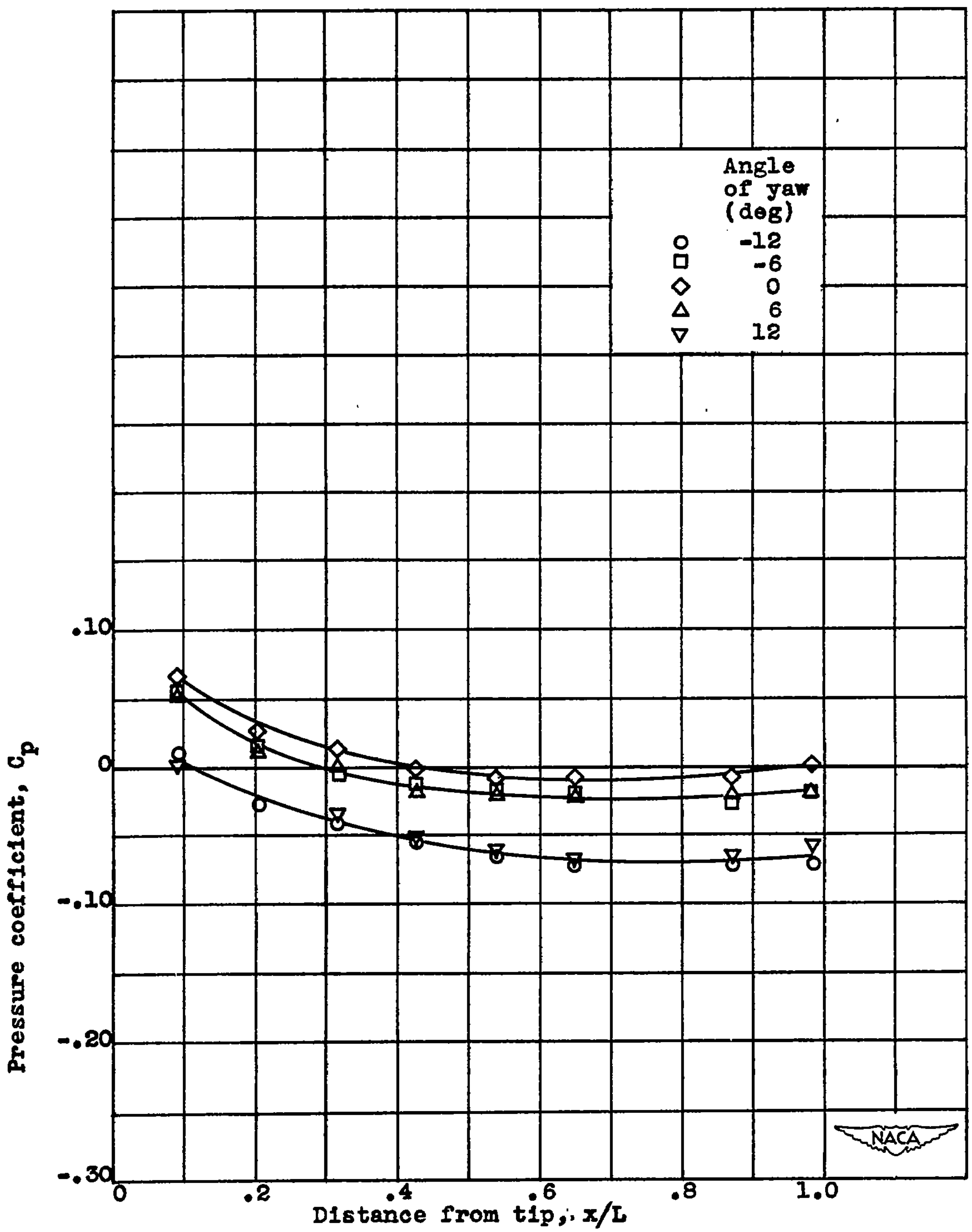
Figure 6. - Pressure distributions along longitudinal planes at 0° angle of attack for range of yaw angles.

1025



(b) $\theta = 45^\circ$ longitudinal plane.

Figure 6. - Continued. Pressure distributions along longitudinal planes at 0° angle of attack for range of yaw angles.

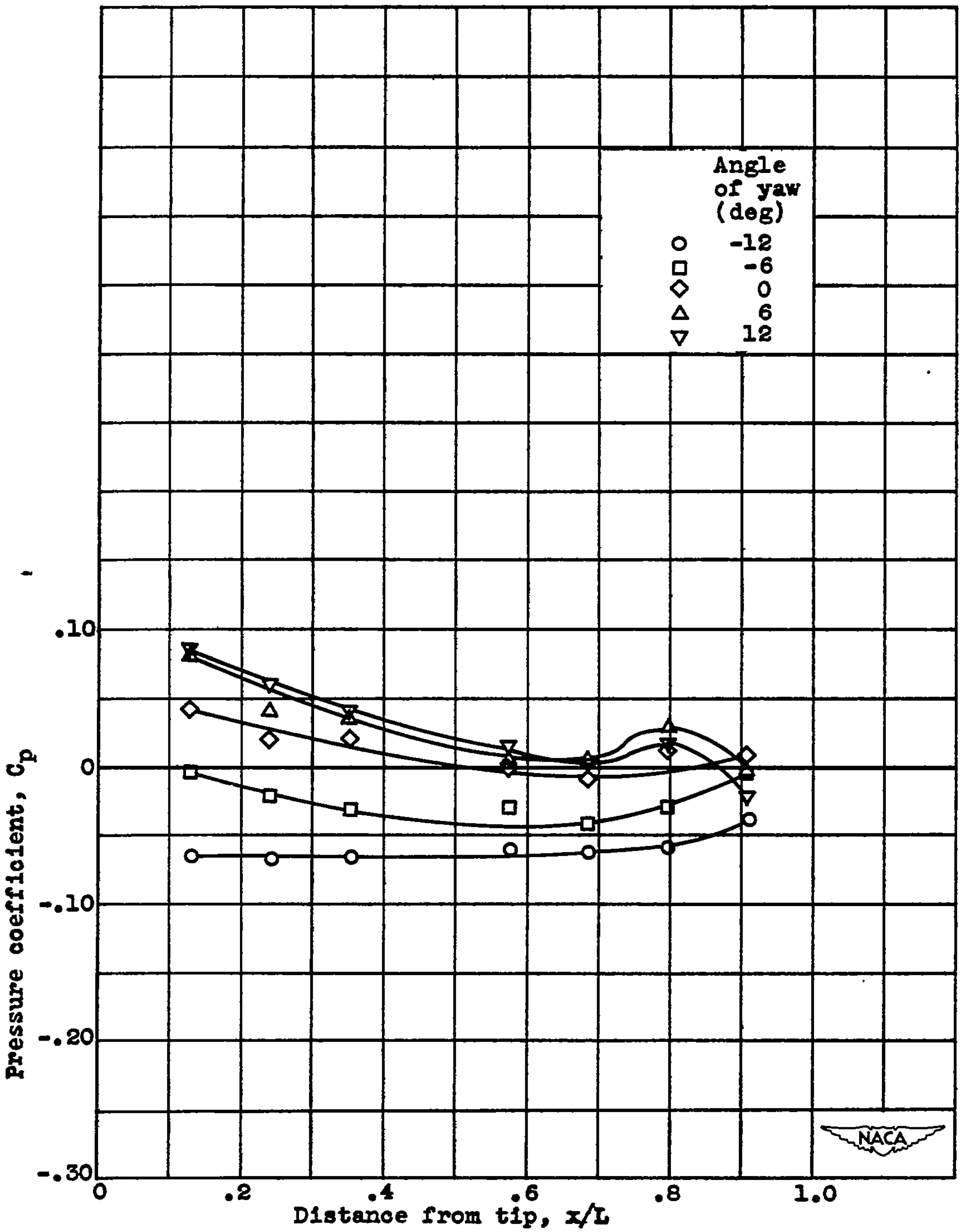


(c) $\theta = 180^{\circ}$ longitudinal plane.

Figure 6. - Continued. Pressure distributions along longitudinal planes at 0° angle of attack for range of yaw angles.

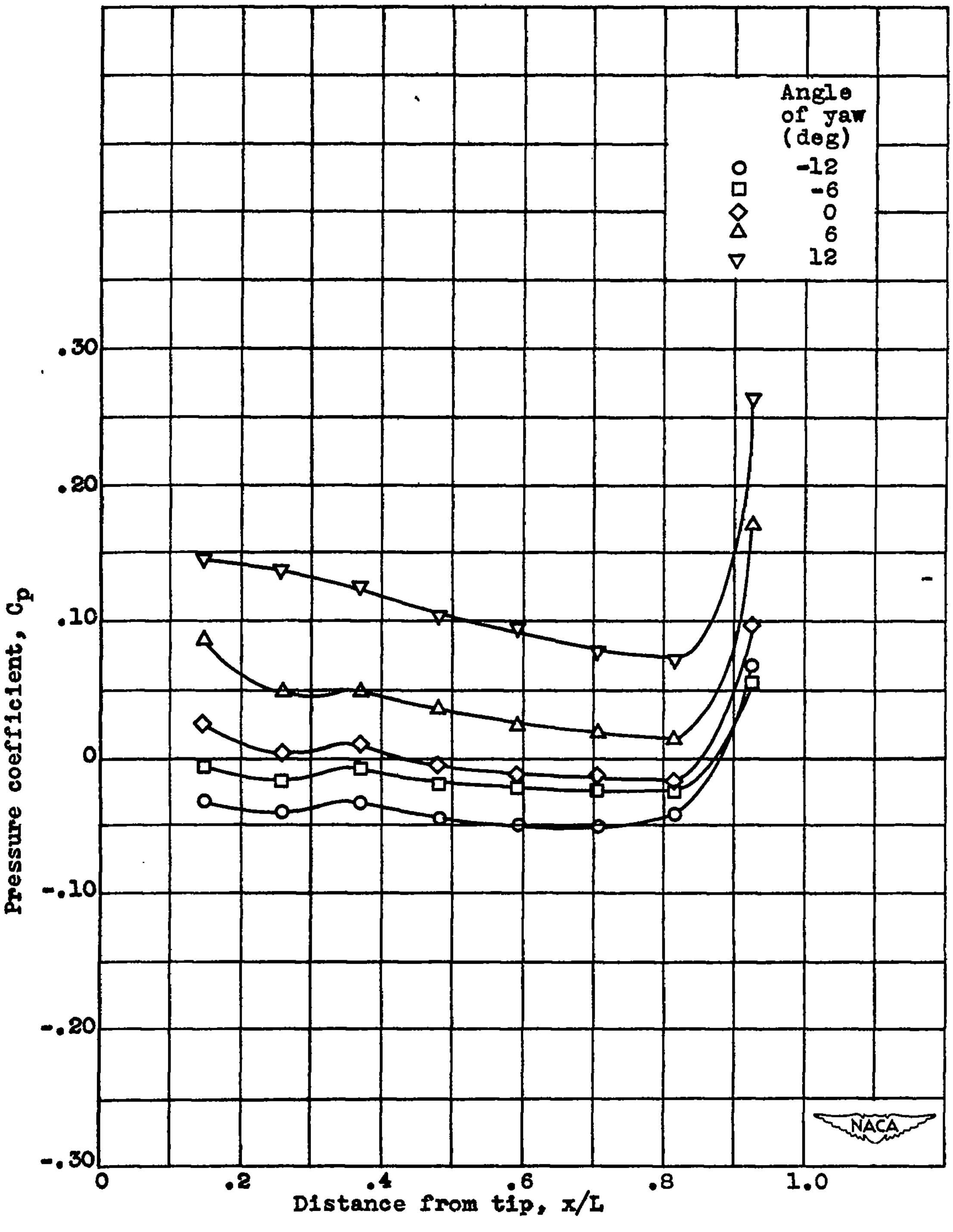
1025

1025



(d) $\theta = 225^\circ$ longitudinal plane.

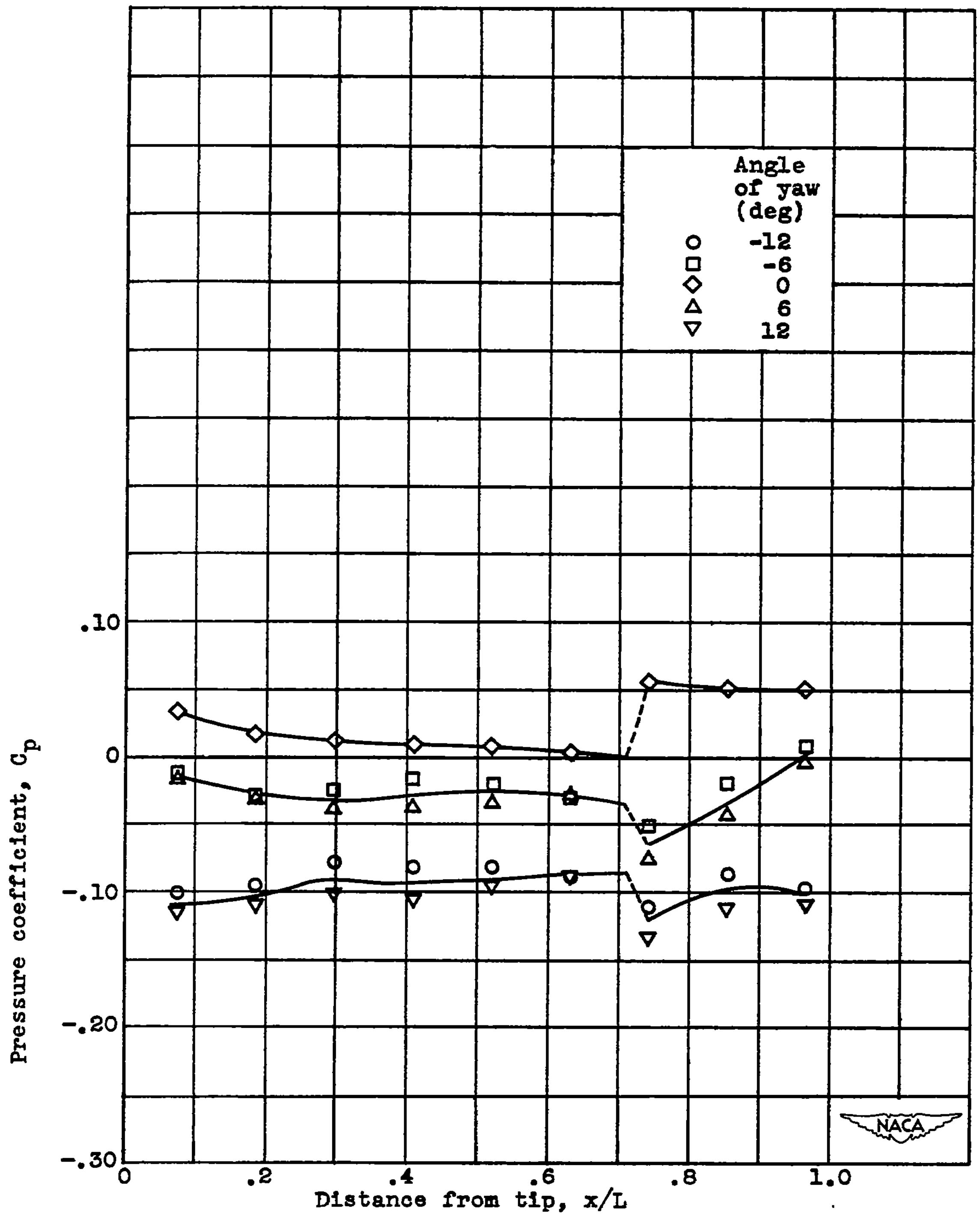
Figure 6. - Continued. Pressure distributions along longitudinal planes at 0° angle of attack for range of yaw angles.



(e) $\theta = 270^\circ$ longitudinal plane.

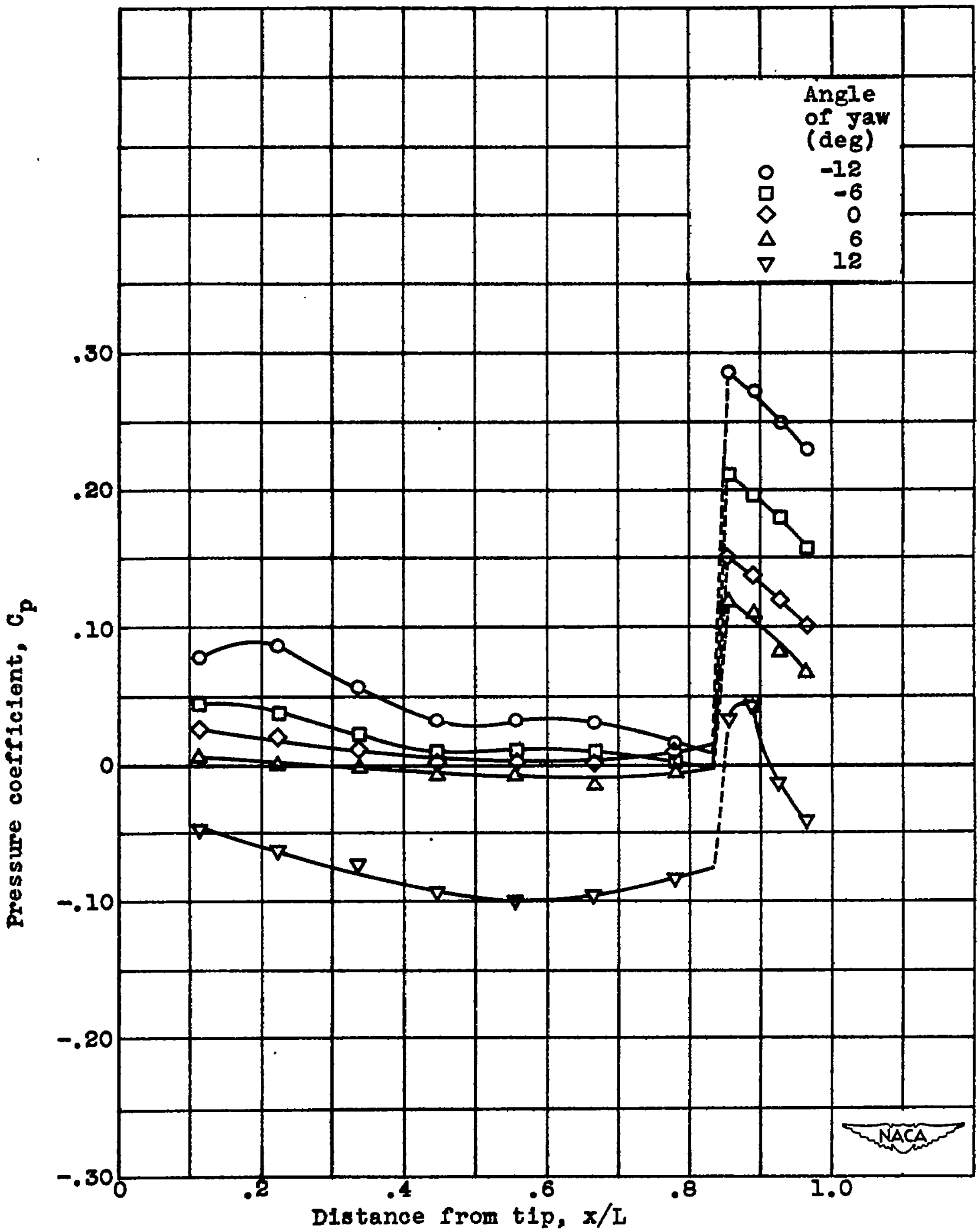
Figure 6. - Concluded. Pressure distributions along longitudinal planes at 0° angle of attack for range of yaw angles.

1025



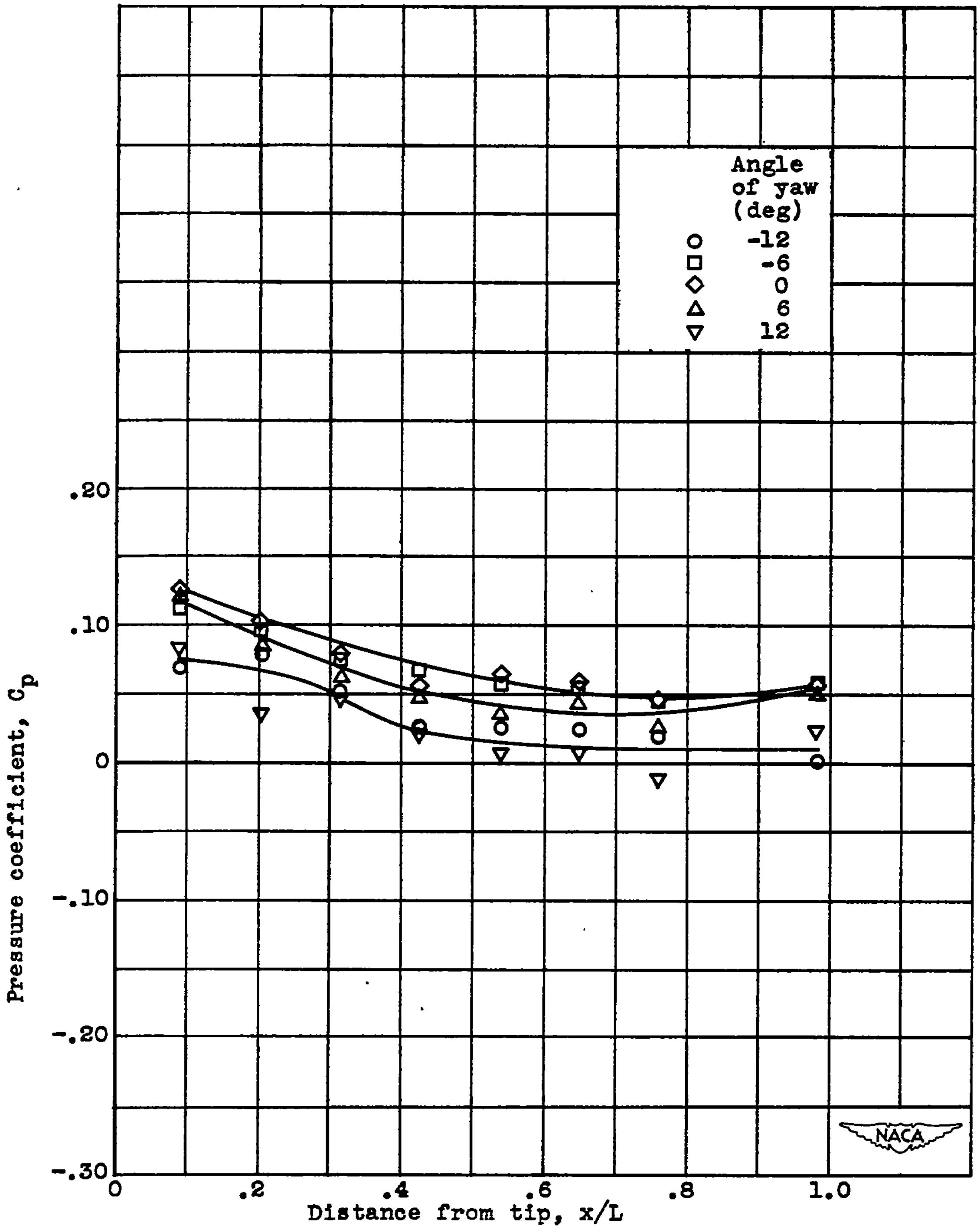
(a) $\theta = 0^\circ$ longitudinal plane.

Figure 7. - Pressure distributions along longitudinal planes at 5° angle of attack for range of yaw angles.



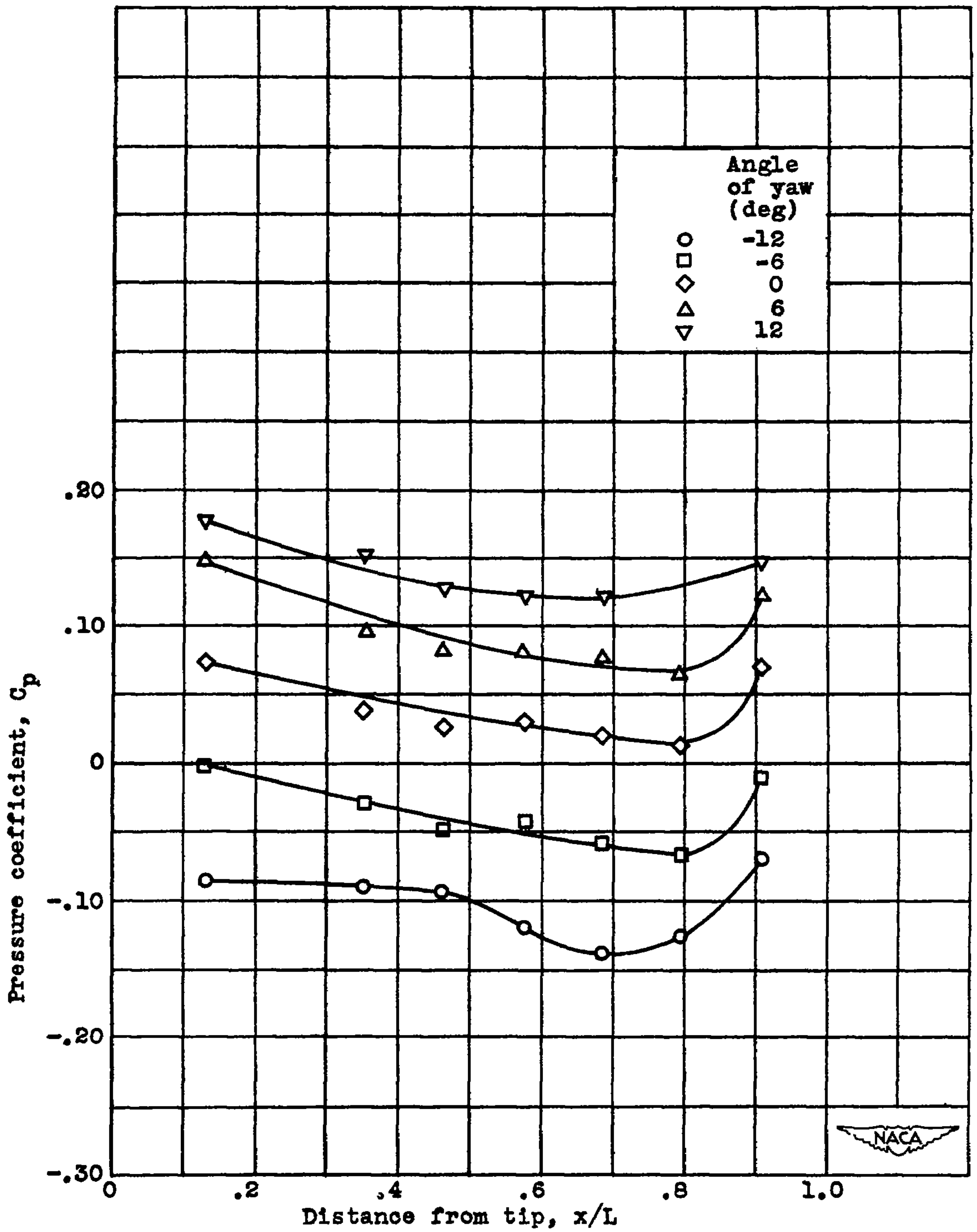
(b) $\theta = 45^\circ$ longitudinal plane.

Figure 7. - Continued. Pressure distributions along longitudinal planes at 5° angle of attack for range of yaw angles.



(c) θ = 180° longitudinal plane.

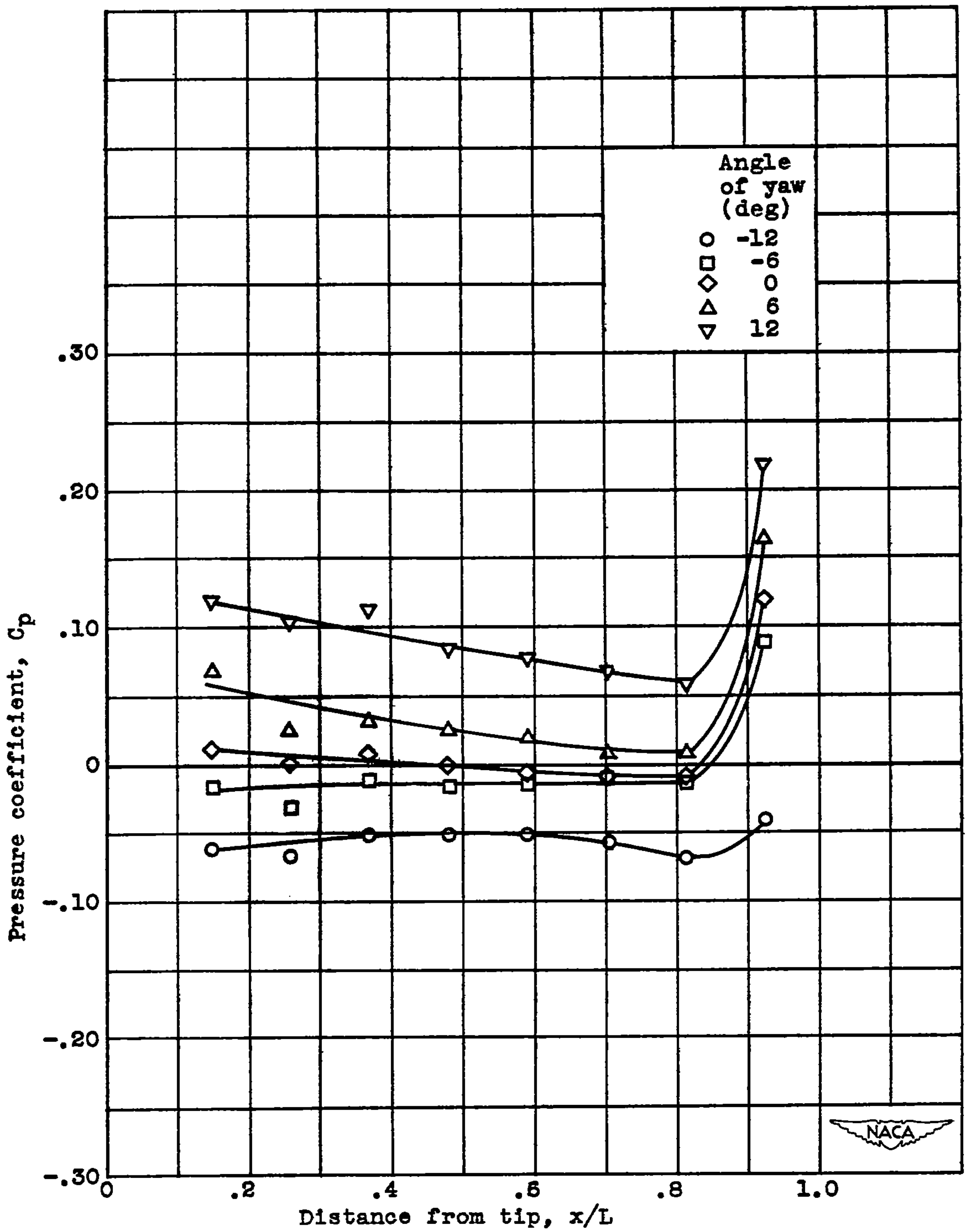
Figure 7. - Continued. Pressure distributions along longitudinal planes at 5° angle of attack for range of yaw angles.



(d) θ = 225° longitudinal plane.

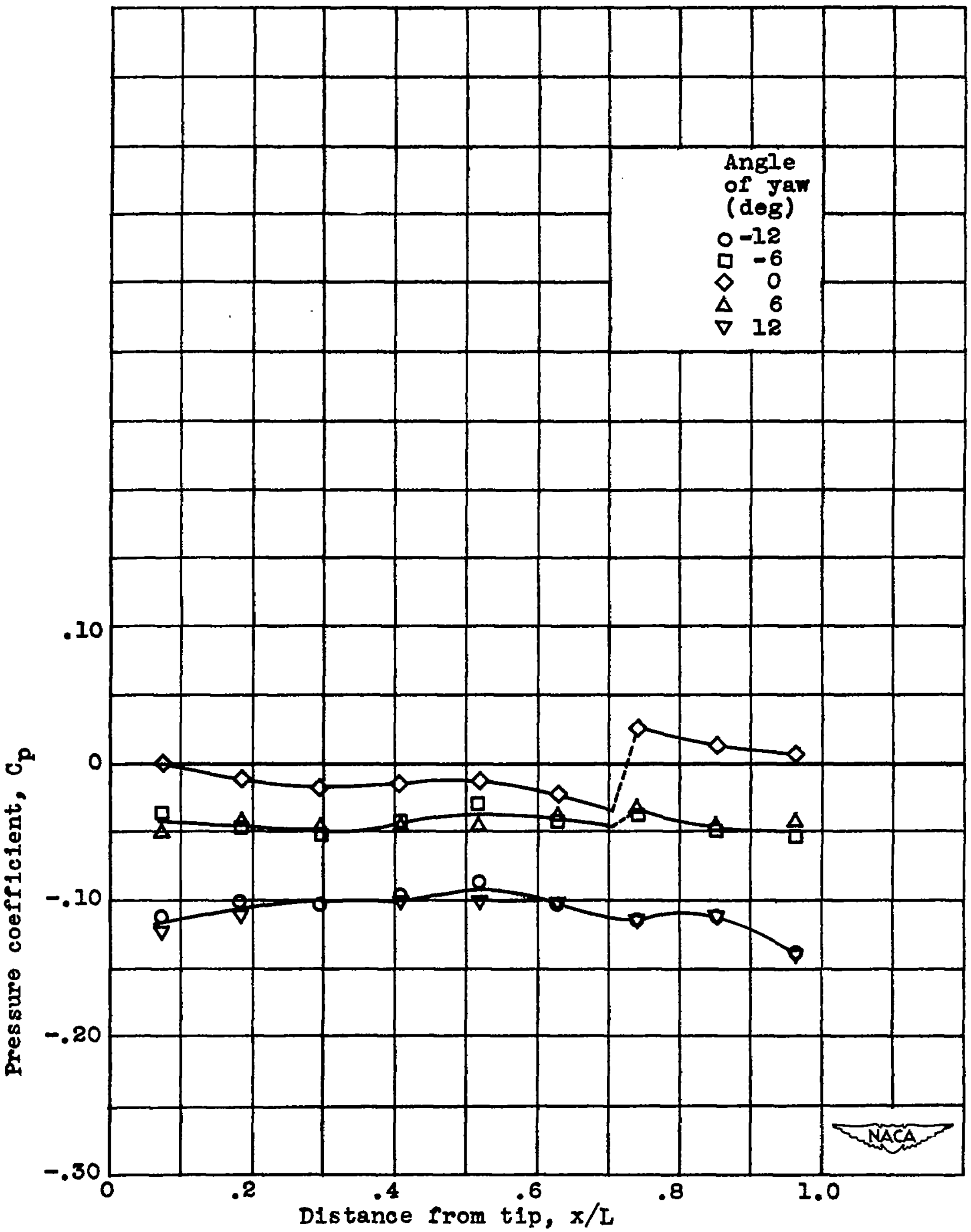
Figure 7. - Continued. Pressure distributions along longitudinal planes at 5° angle of attack for range of yaw angles.

1025



(e) $\theta = 270^{\circ}$ longitudinal plane.

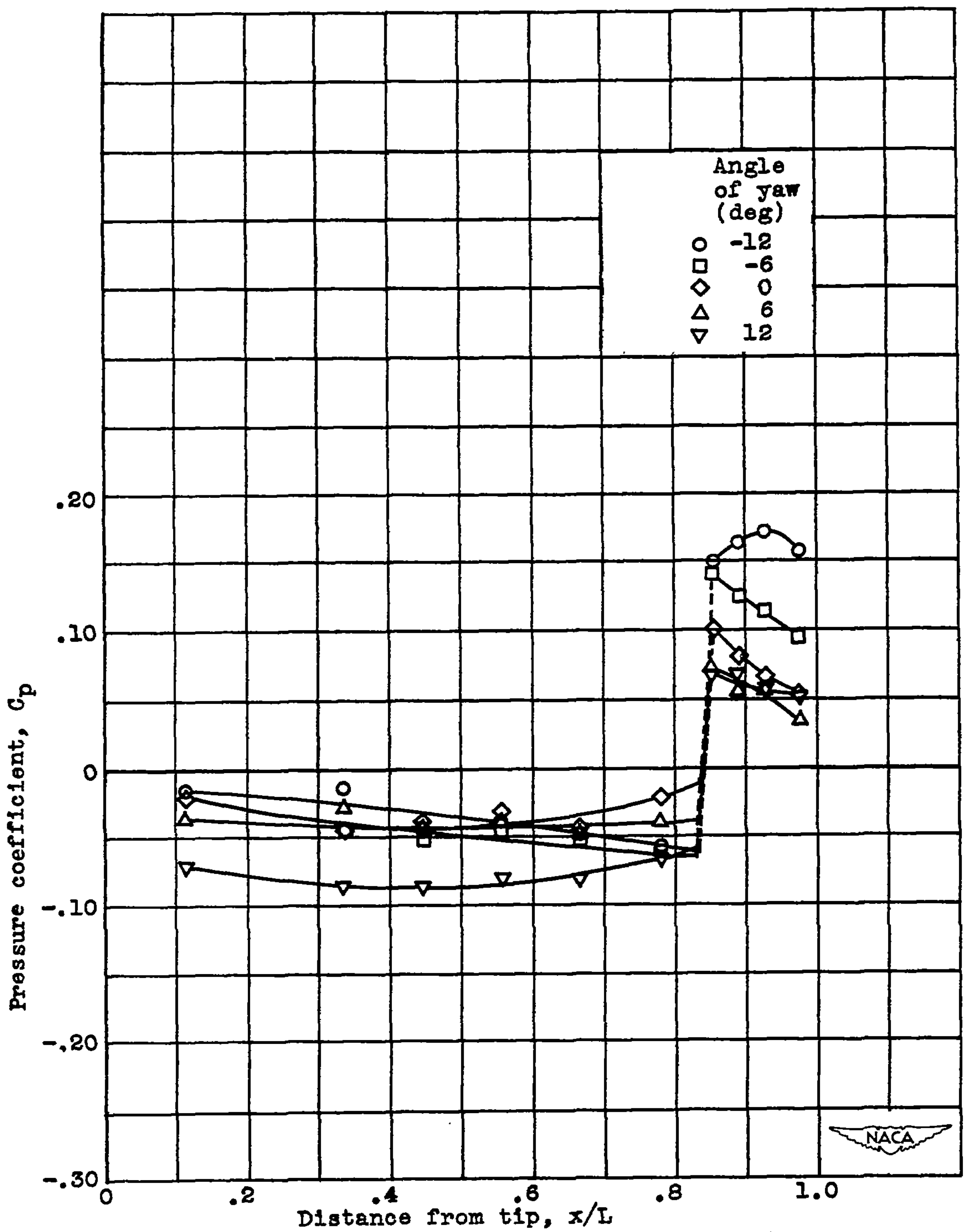
Figure 7. - Concluded. Pressure distributions along longitudinal planes at 5° angle of attack for range of yaw angles.



(a) $\theta = 0^\circ$ longitudinal plane.

Figure 8. - Pressure distributions along longitudinal planes at 10° angle of attack for range of yaw angles.

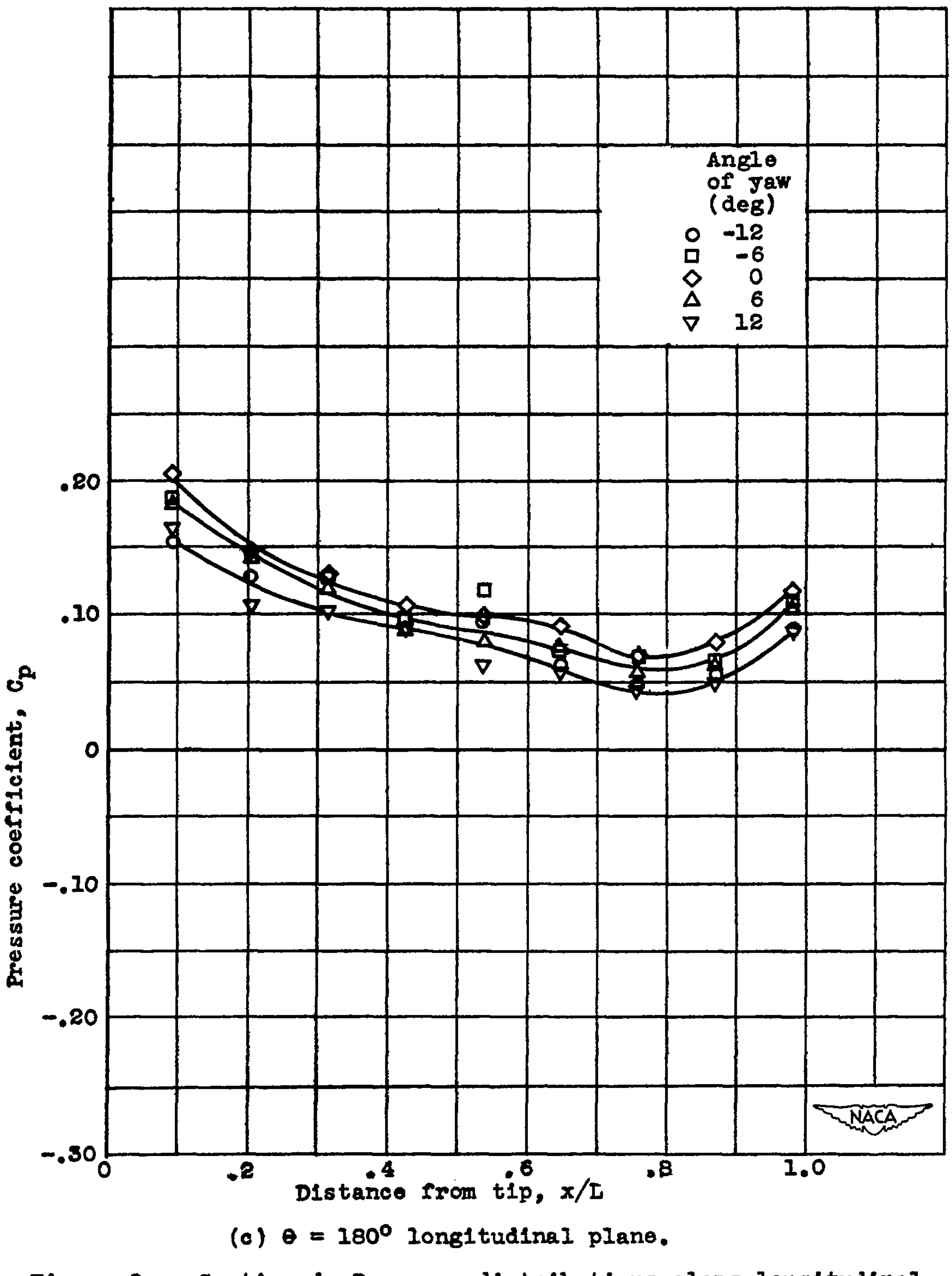
1025



(b) $\theta = 45^{\circ}$ longitudinal plane.

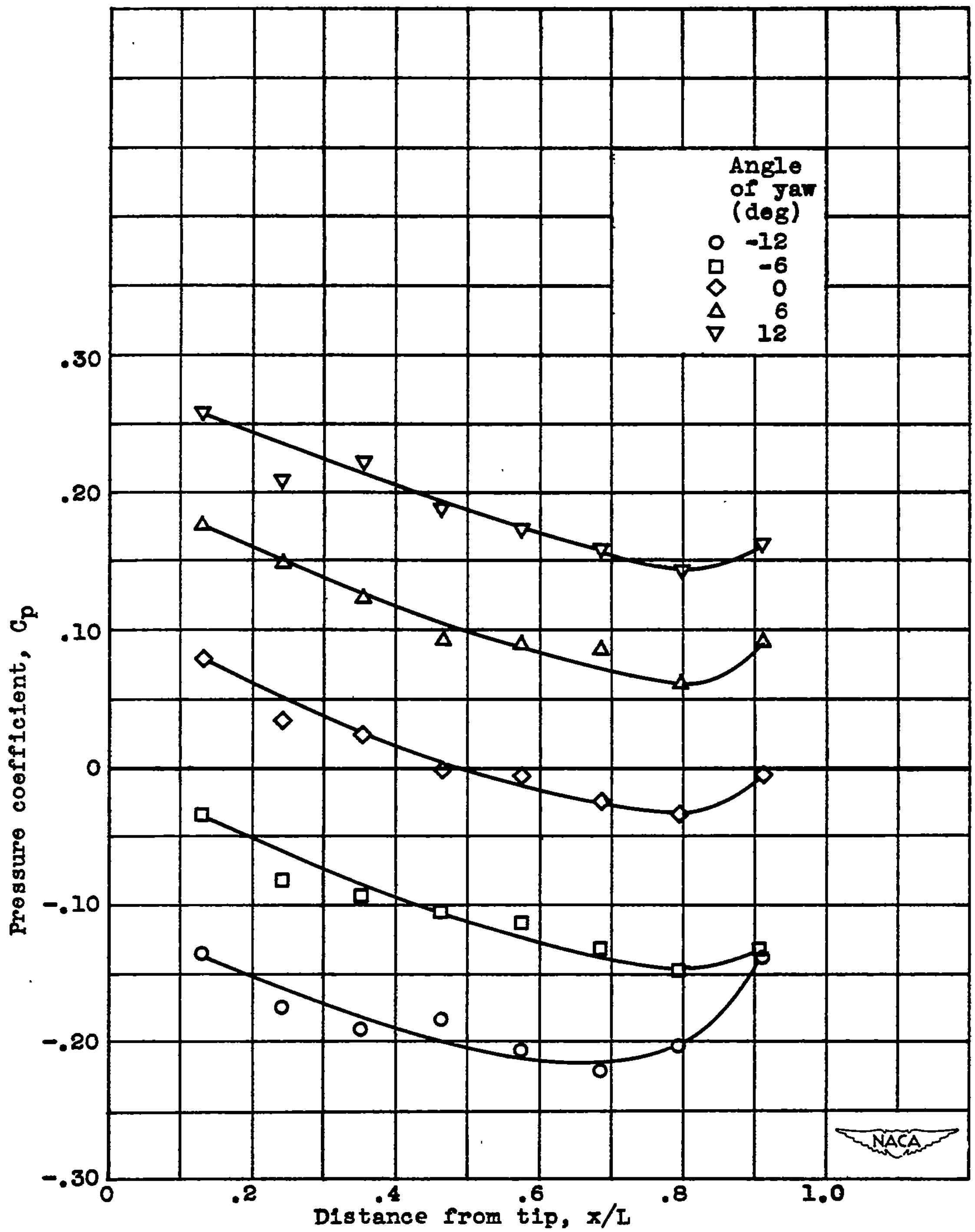
Figure 8. - Continued. Pressure distributions along longitudinal planes at 10° angle of attack for range of yaw angles.

1025



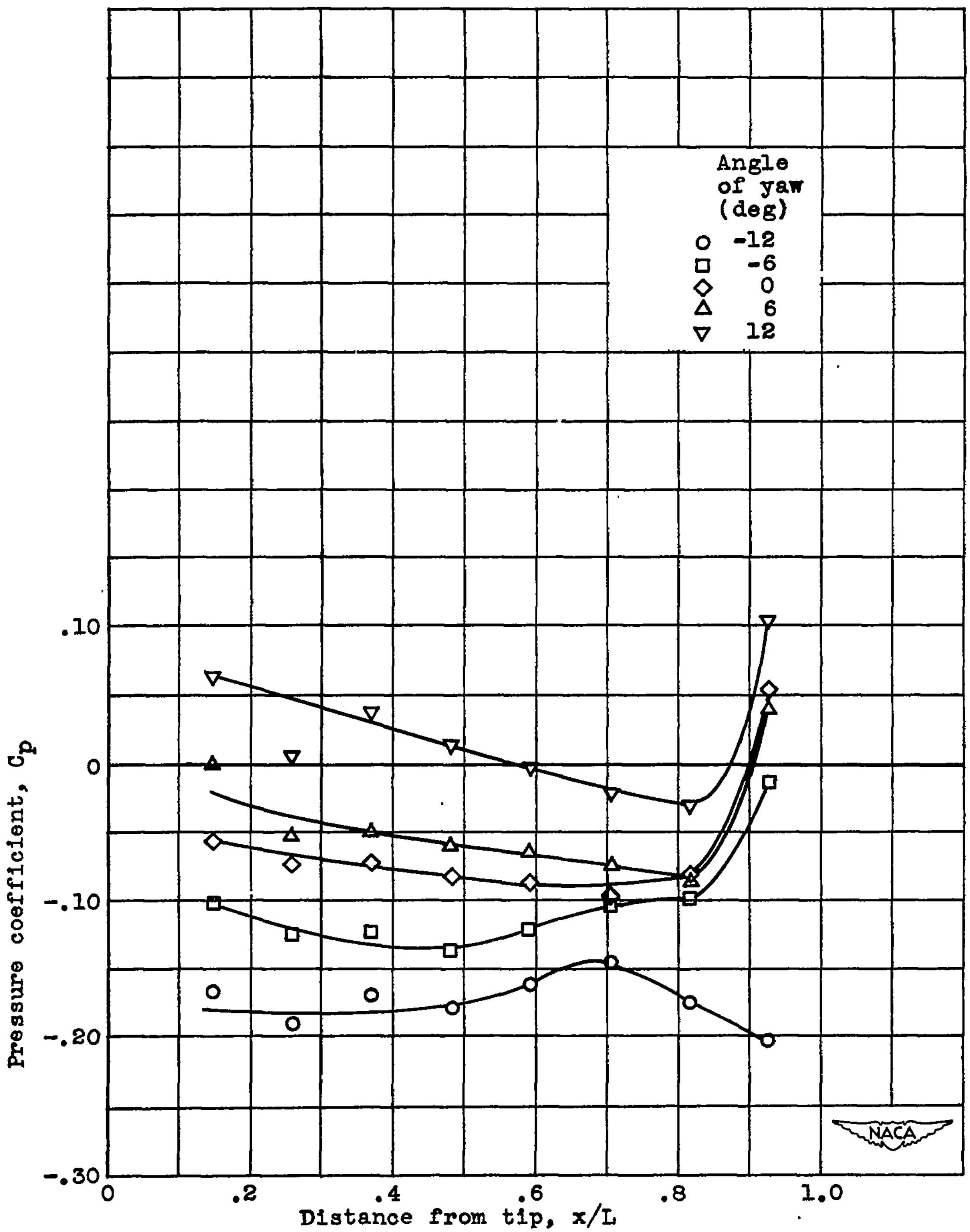
(c) $\theta = 180^{\circ}$ longitudinal plane.

Figure 8. - Continued. Pressure distributions along longitudinal planes at 10° angle of attack for range of yaw angles.



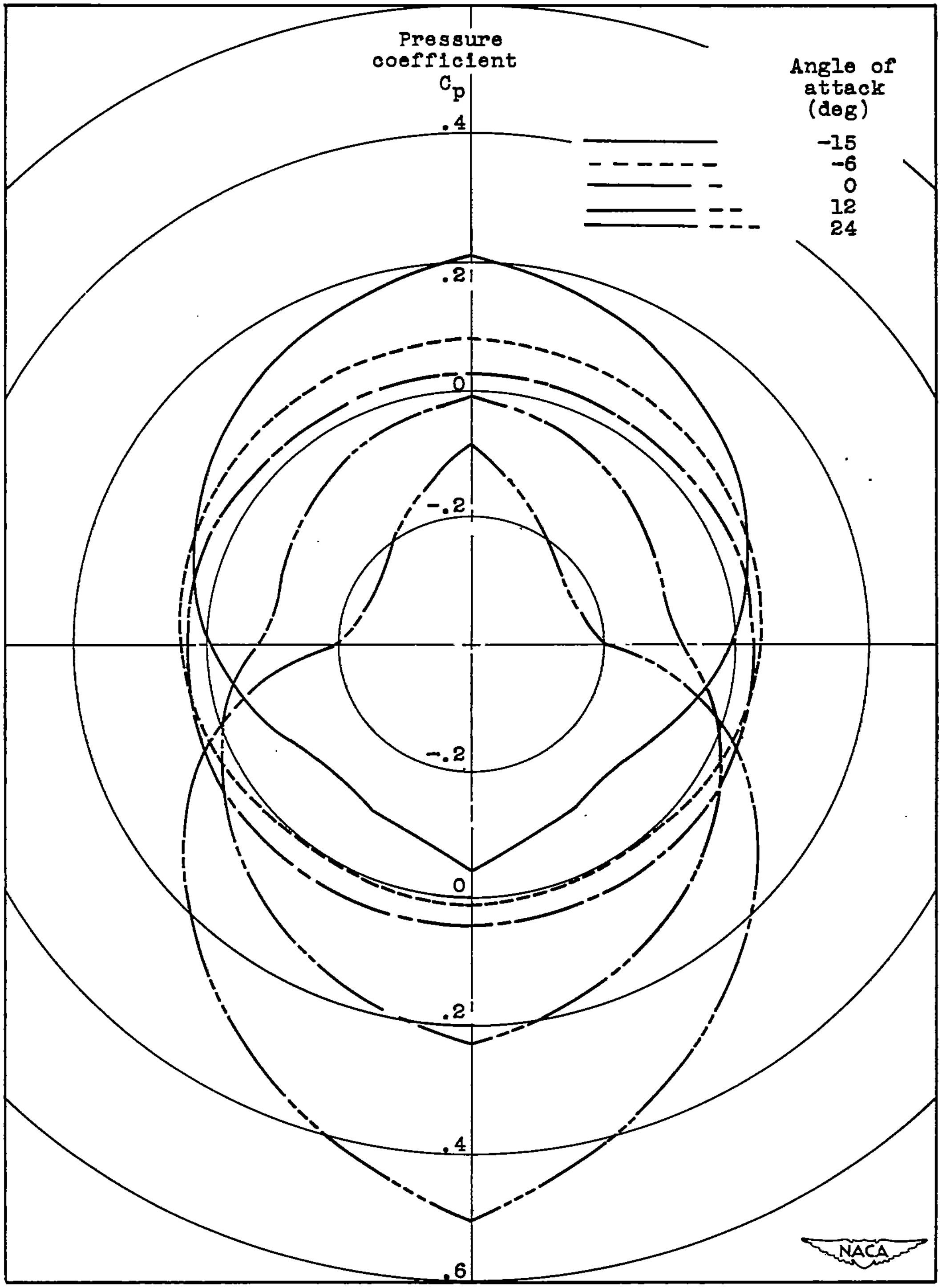
(d) $\theta = 225^{\circ}$ longitudinal plane.

Figure 8. - Continued. Pressure distributions along longitudinal planes at 10° angle of attack for range of yaw angles.



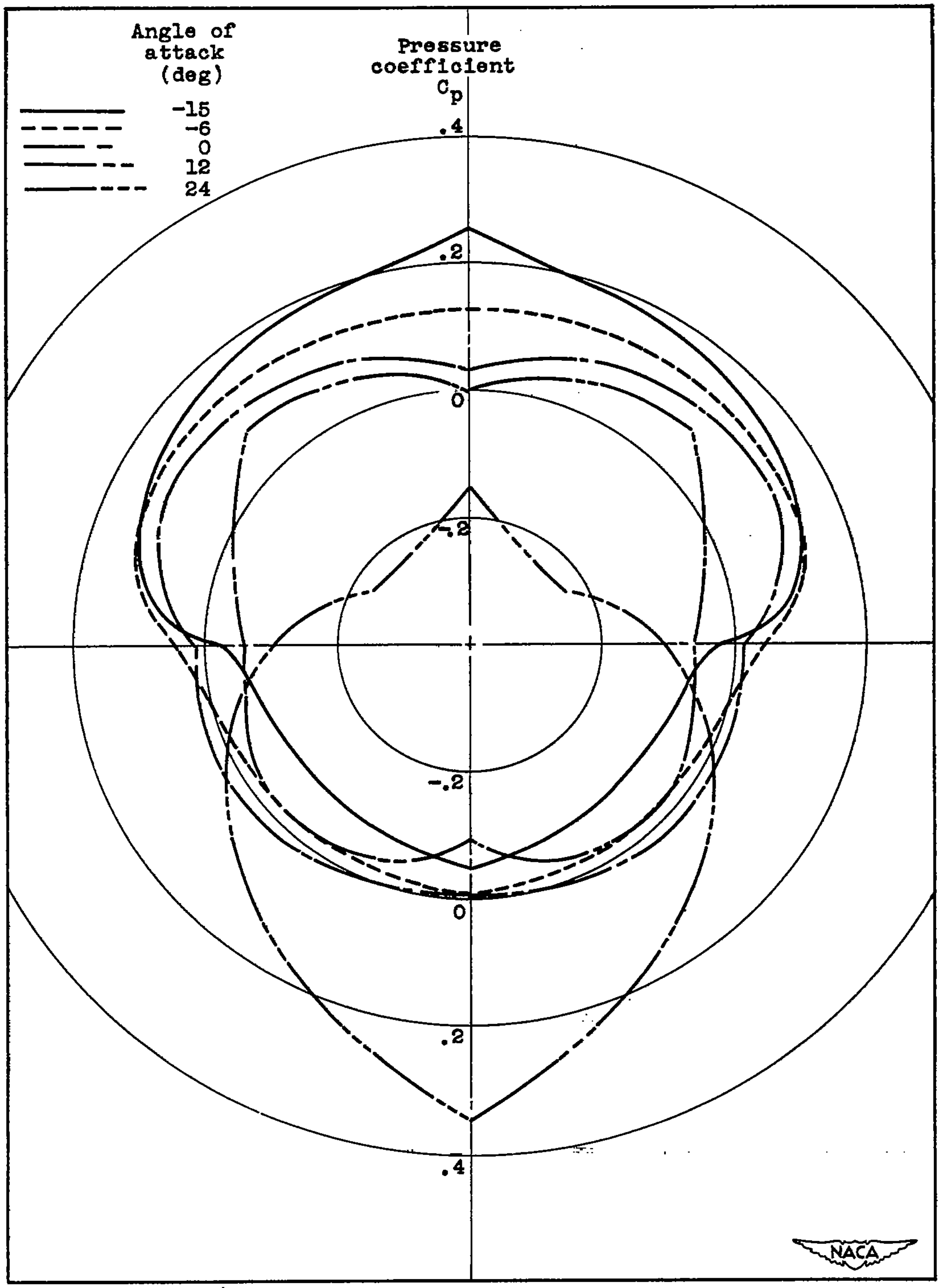
(e) $\theta = 270^\circ$ longitudinal plane.

Figure 8. - Concluded. Pressure distributions along longitudinal planes at 10° angle of attack for range of yaw angles.



(a) $x/L = 0.148$.

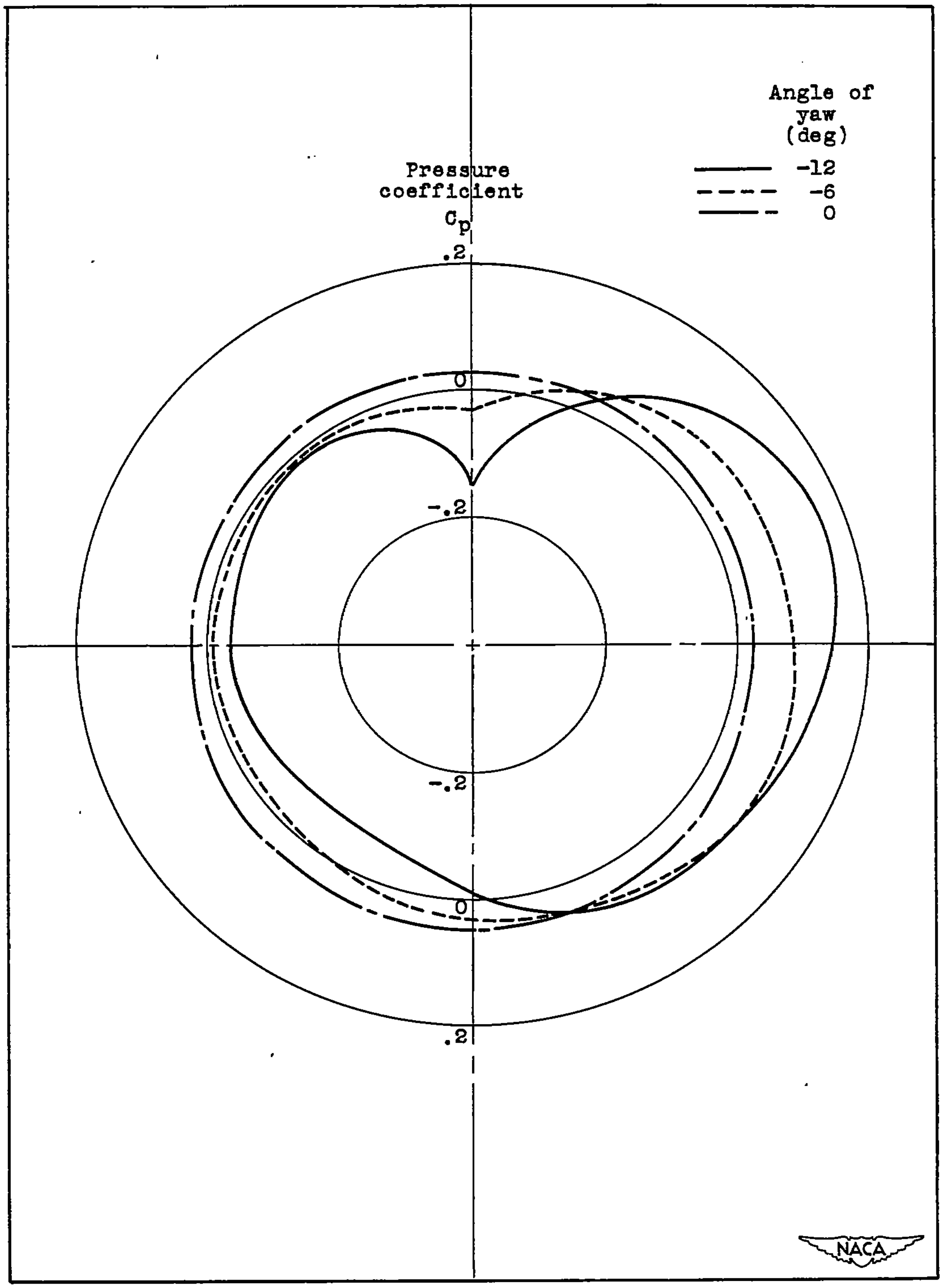
Figure 9. - Radial pressure distributions at 0° yaw angle for various angles of attack.



(b) $x/L = 0.898$.

Figure 9. - Concluded. Radial pressure distributions at 0° yaw angle for various angles of attack.

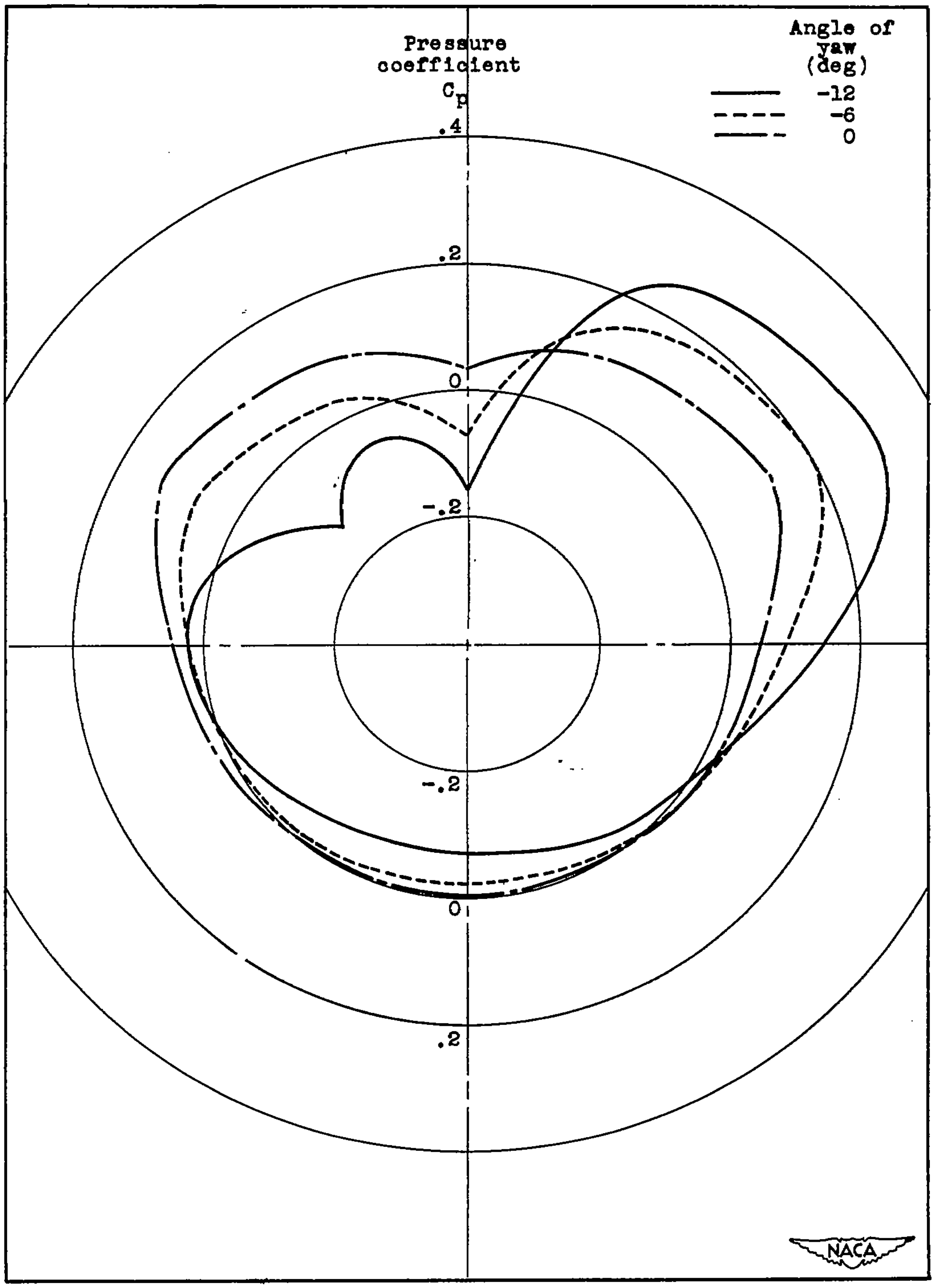
1025



(a) $x/L = 0.148$.

Figure 10. - Radial pressure distributions at 0° angle of attack for three yaw angles.

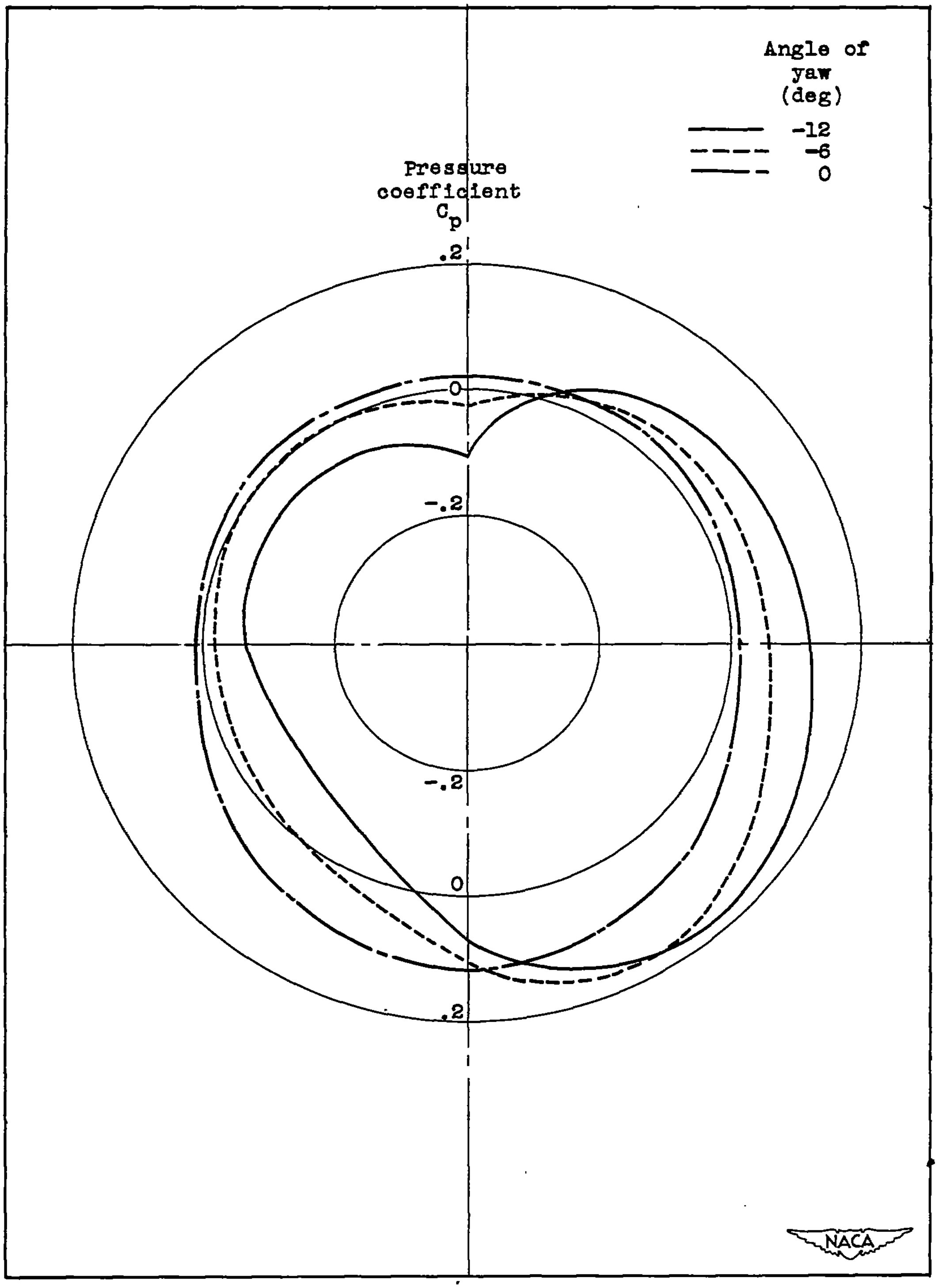
1025



(b) x/L = 0.898.

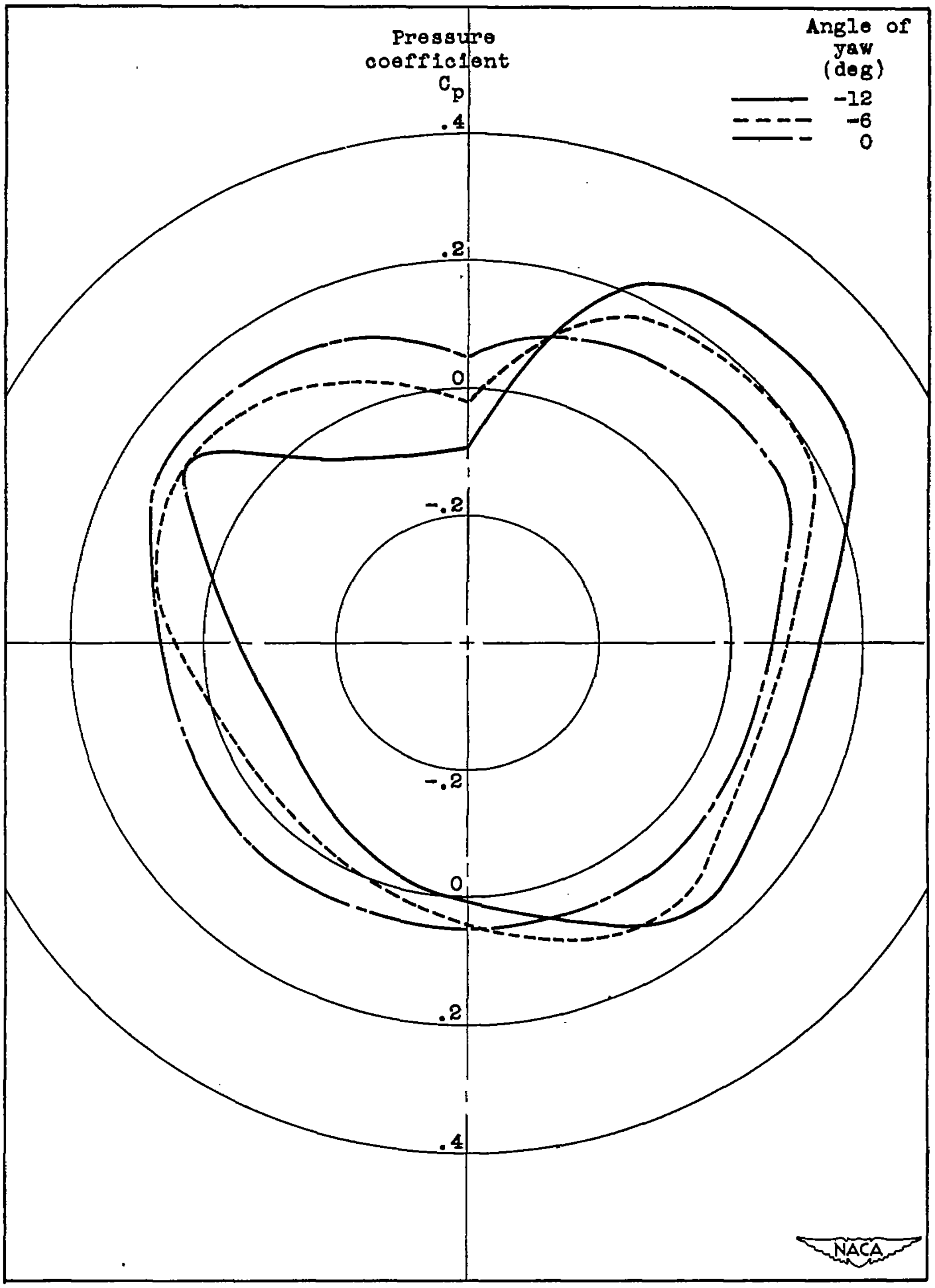
Figure 10. - Concluded. Radial pressure distributions at 0° angle of attack for three yaw angles.

1025



(a) x/L = 0.148.

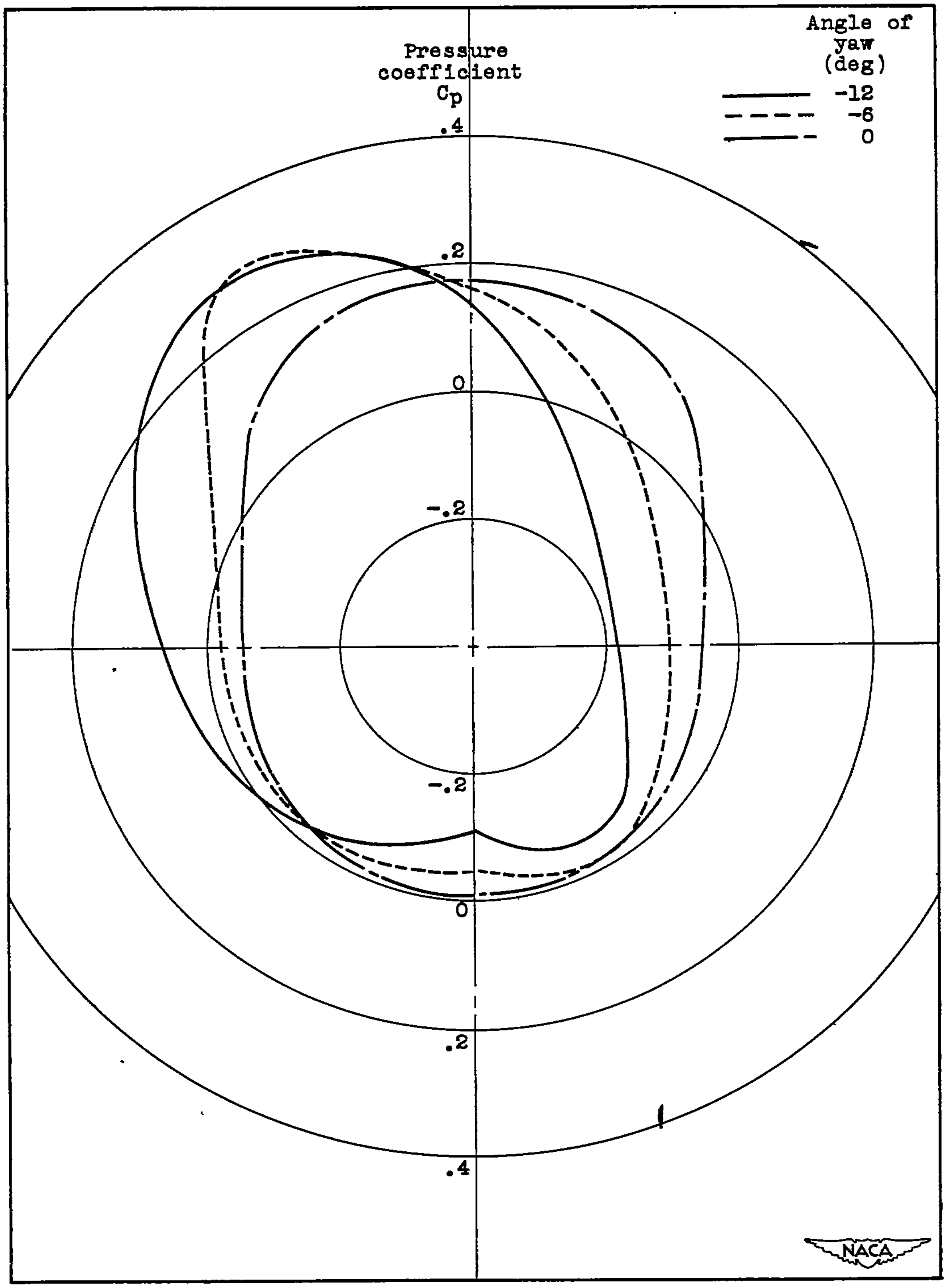
Figure 11. - Radial pressure distributions at 5° angle of attack for three yaw angles.



(b) x/L = 0.898.

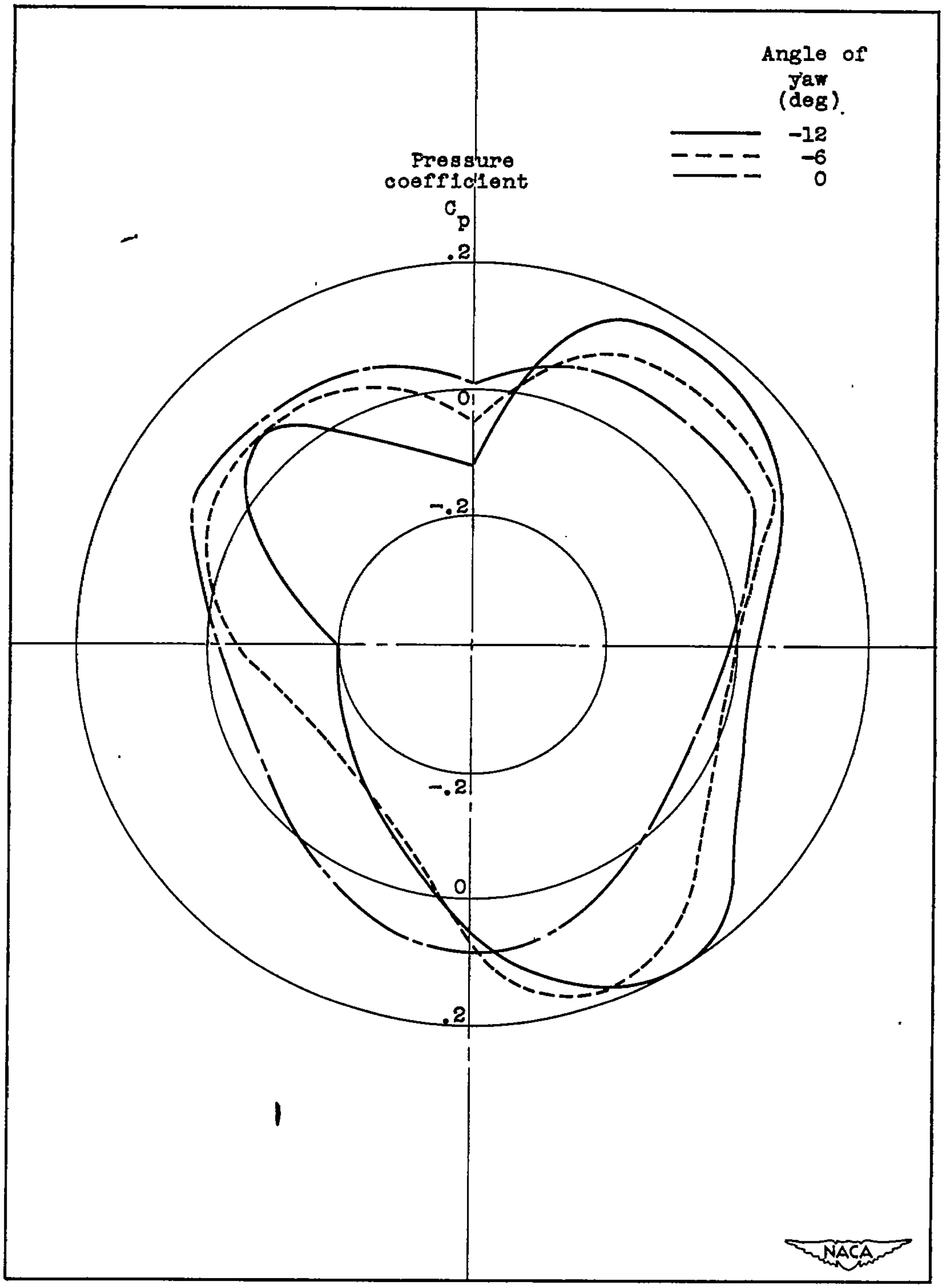
Figure 11. - Concluded. Radial pressure distributions at 5° angle of attack for three yaw angles.

1025



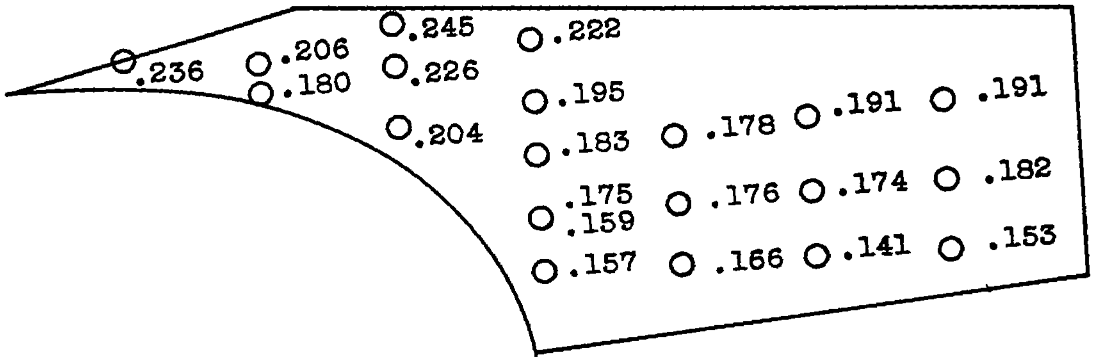
(a) x/L = 0.148.

Figure 12. - Radial pressure distributions at 10° angle of attack for three yaw angles.

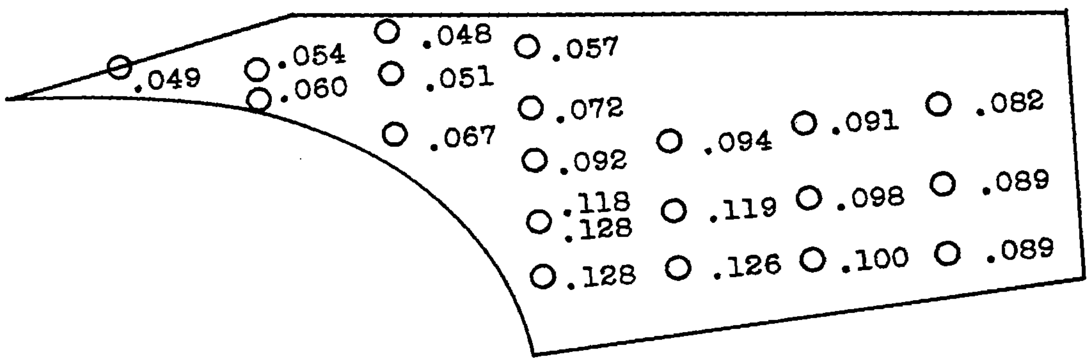


(b) x/L = 0.898.

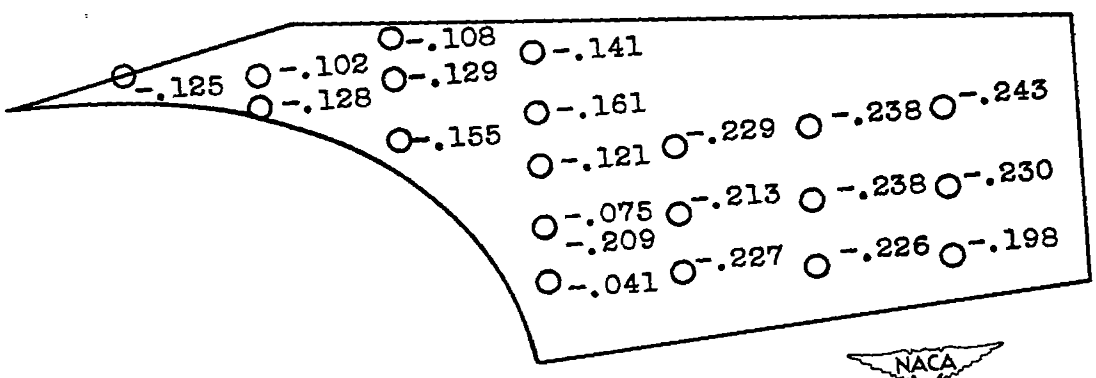
Figure 12. - Concluded. Radial pressure distributions at 10° angle of attack for three yaw angles.



(a) Angle of attack, -15°.

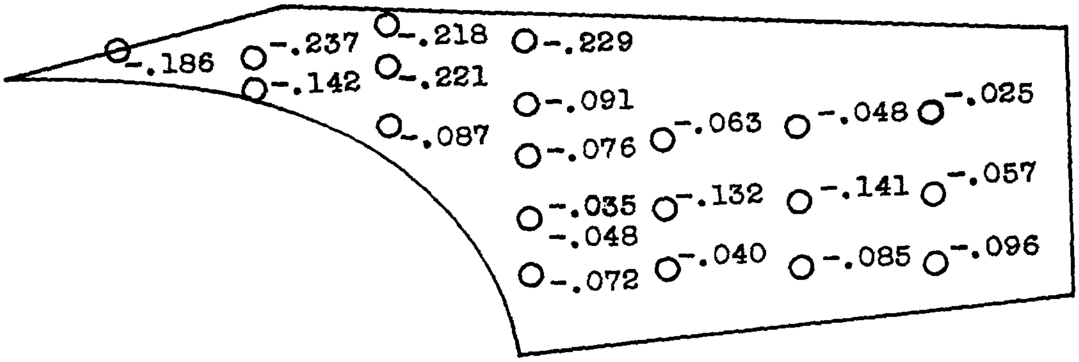


(b) Angle of attack, 0°.

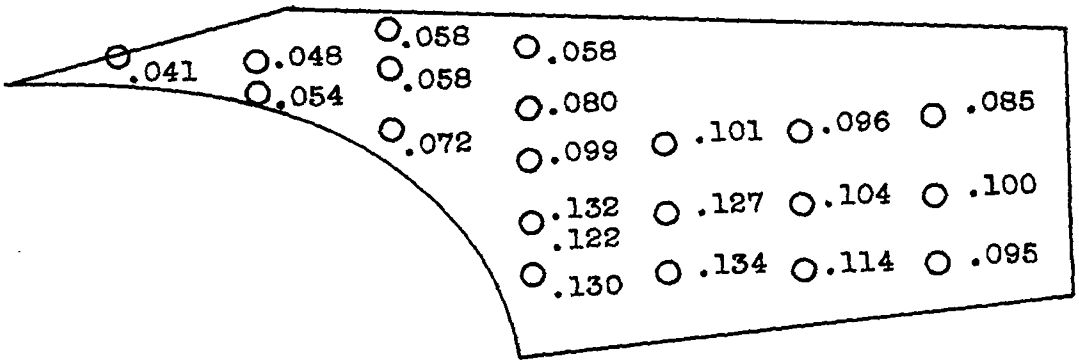


(c) Angle of attack, 24°.

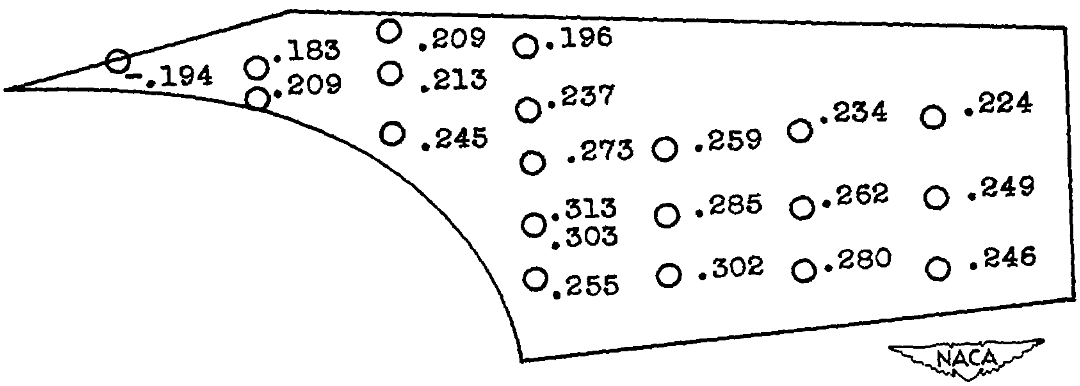
Figure 13. - Pressure coefficients on wedge surface at 0° angle of yaw for three angles of attack.



(a) Angle of yaw, -12°.

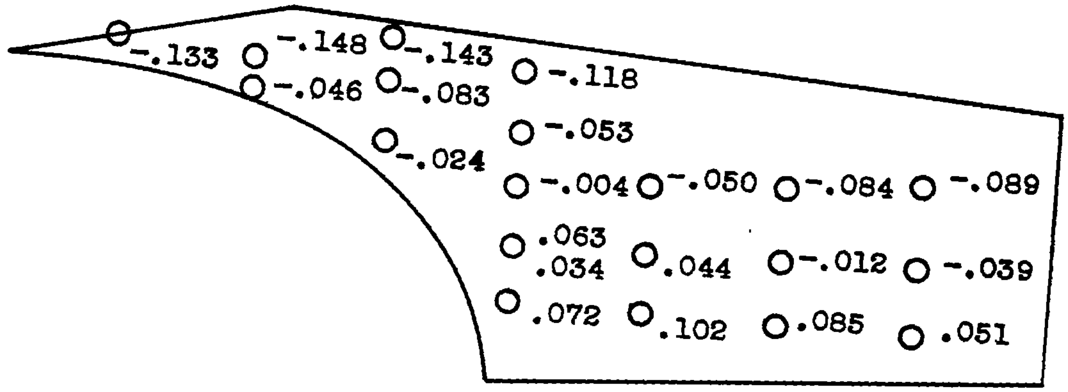


(b) Angle of yaw, 0°.

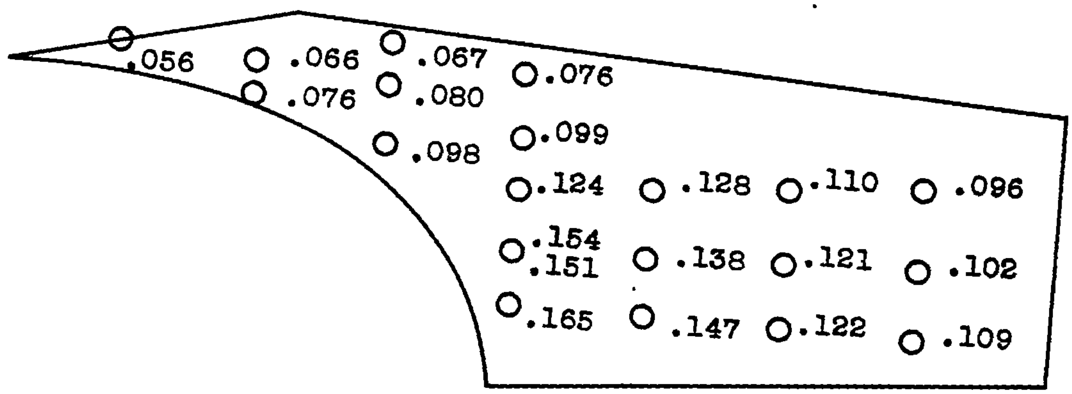


(c) Angle of yaw, 12°.

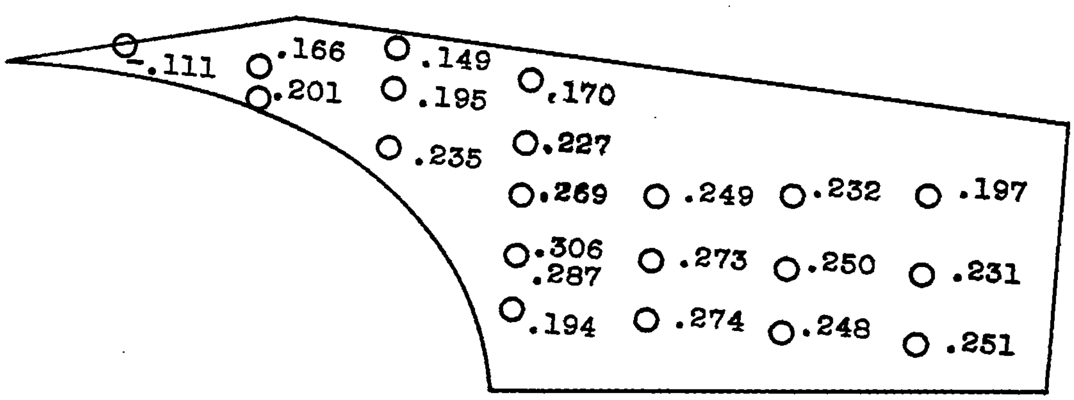
Figure 14. - Pressure coefficients on wedge surface at 0° angle of attack for three angles of yaw.



(a) Angle of yaw, -12°.

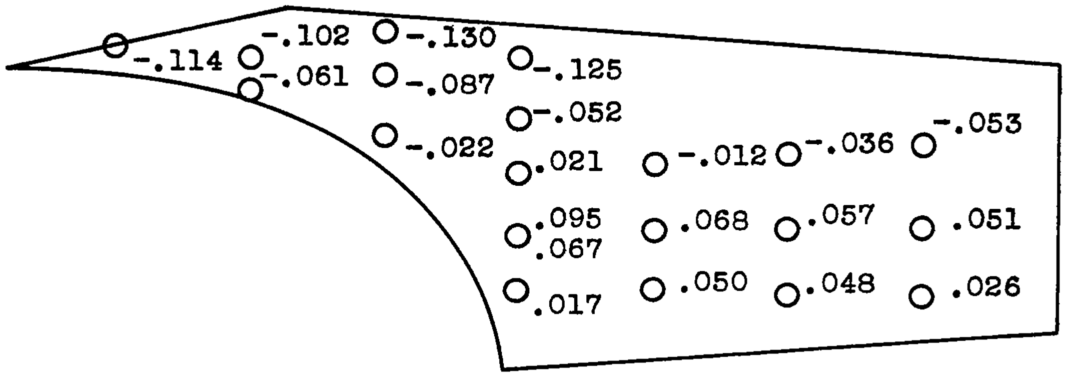


(b) Angle of yaw, 0°.

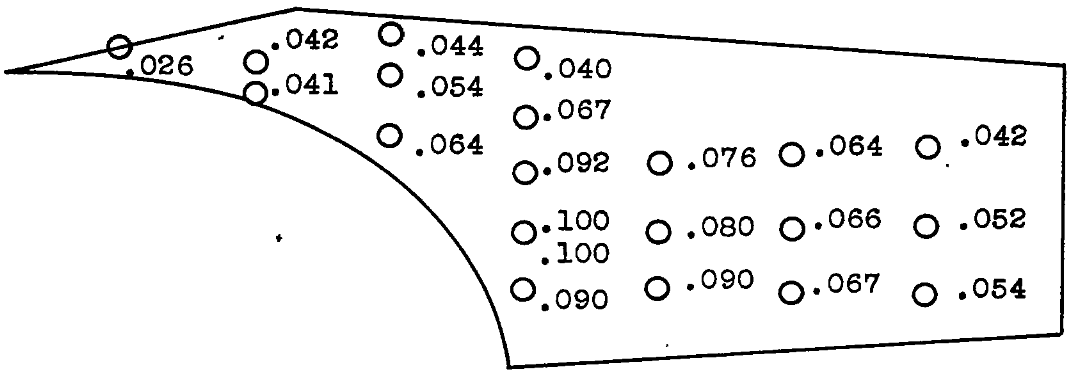


(c) Angle of yaw, 12°.

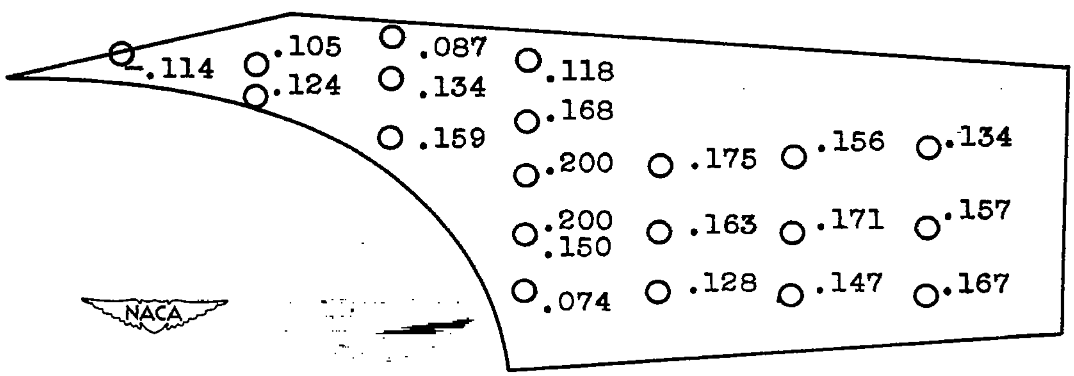
Figure 15. - Pressure coefficients on wedge surface at 5° angle of attack for three angles of yaw.



(a) Angle of yaw, -12°.



(b) Angle of yaw, 0°.



(c) Angle of yaw, 12°.

Figure 16. - Pressure coefficients on wedge surface at 10° angle of attack for three angles of yaw.